

SINGLE STAGE EXPERIMENTAL EVALUATION OF HIGH MACH NUMBER COMPRESSOR ROTOR BLADING PART 4 - PERFORMANCE OF ROTOR 2D

by

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prepared for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

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LYNN, MASSACHUSETTS/CINCINNATI, OHIO

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PART 4 - PERFORMANCE OF ROTOR 2D

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ABSTRACT

A 1400 foot per second tip speed rotor with a 0.5 hub-tip radius ratio and double-circular-arc blade sections, designed to deliver a total pressure ratio of 1.76 and a rotor adiabatic efficiency of 0.837 at a flow of 215.49 lbs/sec, was tested with uniform inlet flow. For a point at design speed, judged to have adequate stall margin for engine operation, a rotor total pressure ratio of 1.677 and an adiabatic efficiency of 0.854 at a flow of 226.0 lbs/sec were actually achieved.

SUMMARY

A 1400 foot per second tip speed rotor, designed to have a diffusion factor of 0.45 at the tip, was tested with uniform inlet flow. A double-circulararc blade element design was used for the entire blade height. The hub-tip radius ratio at rotor inlet is 0.50. Neither inlet guide vanes nor a stator row were employed.

The rotor was designed to deliver a total-pressure ratio of 1.76 and a rotor adiabatic efficiency of 0.837 at a flow of 215.49 lbs/sec. For a point at design speed, judged to have adequate stall margin for engine operation, a rotor total pressure ratio of 1.677 and a rotor adiabatic efficiency of 0.854 at a flow of 226.0 lbs/sec were actually achieved. Peak rotor adiabatic efficiencies of 0.950, 0.958, 0.917, 0.875, and 0.814 were obtained at 50, 70, 90, 100 and 110 percent of design speed, respectively.

Blade element data were obtained from measurements over a range of speeds from 50% to 110% design speed. Results of these blade element measurements were used to show the variation of deviation angle, diffusion factor and loss coefficient as a function of incidence angle for five radial immersions. The rotor was also stalled at these speeds and overall performance data were obtained while in stall. The stall type was rotating stall at all speeds.

INTRODUCTION

In the early 1950's a test program was initiated at the NACA Lewis Laboratory to provide blade element data for double-circular-arc airfoil sections to be applied to the design of transonic rotors (ref. 1). Available experimental

and analytical data indicated that such airfoils produced a good chordwise loading and could be used in transonic compressors with resulting high efficiencies at relative Mach numbers up to 1.2 (ref. 2).

During the last fifteen years the development of axial-flow compressors for todays' aircraft engines has resulted in high blade speeds and stage loadings. This leads to higher relative Mach numbers and can cause severe efficiency penalties due to the presence of shocks. It is the purpose of the current experimental program to determine the performance potential of such rotors and to obtain data that will aid in the selection of optimum blade sections.

A new type of blade shape has been employed in general for this test series. The camber line consists of two circular arcs that are mutually tangent at the point where they join. The front arc is identified as the supersonic arc, and the rear arc is identified as the subsonic arc. The term, camber ratio, refers to the ratio of the camber of the supersonic arc to the total camber. Blade elements developed in this way are called multiple-circular-arc elements; the double-circular-arc airfoil is a particular case in which the supersonic arc and the subsonic arc have the same curvature. Rotor 2D, the third of four medium-aspect-ratio rotors, has such a double-circular-arc section along the entire span. The blade shape thus represents a link between the present series of tests and the earlier NACA series. The double-circular-arc tip element has a camber ratio of 0.65 and a diffusion factor of 0.45.

Details of the design of this rotor and the other rotors to be evaluated are given in reference 3. This report presents overall performance and blade-element results of tests on Rotor 2D with a uniform inlet flow.

SYMBOLS

The following symbols are used in this report:

A flow area, in²

A area represented by each discharge rake element. This is the area of an annulus bounded either by radii midway between those of two adjacent elements or by the hub or casing, in

a distance along chord line to position where maximum perpendicular displacement between camber line and chord line occurs, in

C_h enthalpy-equivalent static-pressure-rise coefficient,

$$c_{h} = \frac{2gJc_{p}t_{1} \left[\left(\frac{p_{2}}{p_{1}} \right)^{\frac{\gamma-1}{\gamma}} - 1 \right] - (u_{2}^{2} - u_{1}^{2})}{v_{1}^{2}}$$

C static-pressure-rise coefficient,

$$c_p = \frac{p_2 - p_1}{p_1' - p_1}$$

c blade-chord length, in

c specific heat at constant pressure, Btu/lb-°R

D diffusion factor,

$$D = 1 - \frac{V_{1}'}{V_{1}'} + \frac{r_{2}V_{\theta 2} - r_{1}V_{\theta 1}}{2r_{0}V_{1}'}$$

g acceleration due to gravity, 32.174 ft/sec²

i incidence angle, difference between air angle and camber line angle at leading edge in cascade projection, deg

i unit vector in direction of intersection of axisymmetric stream surface and blade mean surface.

J mechanical equivalent of heat, 778.161 ft-lb/Btu

M Mach number

P total or stagnation pressure, psia

P_{in} compressor inlet average total pressure, psia

? arithmetic average total pressure at j immersion, psia

p static or stream pressure, psia

r radius, in

mean radius, average of streamline leading-edge and trailing-edge radii, in

T total or stagnation temperature, °R

 T_{i} arithmetic average total temperature at j immersion, ${}^{\circ}R$

t static or stream temperature, °R

t blade thickness, in

	^t e	blade edge thickness, in
	t _m	blade maximum thickness, in
•	U	rotor speed, ft/sec
	V	air velocity, ft/sec
	V _{zj}	average axial velocity at j immersion, ft/sec
	w .	weight flow, lb/sec
	Z ,	displacement along compressor axis, in
	β	air angle, angle whose tangent is the ratio of tangential to axial velocity, deg
<i>.</i> '.	Υ	ratio of specific heats
	γ°	blade-chord angle, angle in cascade projection between blade chord and axial direction, deg
• . •	ć	ratio: $\frac{\text{total pressure}}{\text{standard pressure}}$, $\frac{\text{psia}}{14.696 \text{ psia}}$
	δ°	deviation angle, difference between air angle and camber line angle at trailing edge in cascade projection, deg
	€ •	meridional angle, angle between tangent to streamline projected on meridional plane and axial direction, deg
	θ	ratio: $\frac{\text{total temperature}}{\text{standard temperature}}$, $\frac{^{\circ}R}{518.688^{\circ}R}$
	₉ •	angular displacement about compressor axis, deg
	r)	efficiency
	K °	angle between cylindrical projection of i_{κ} and axial direction, deg
	ρ	static or stream density, lb-sec ² /ft ⁴
	Ø	solidity, ratio of chord to spacing
	φ	camber angle, difference between angles in cascade projection of tangents to camber line at extremes of camber line arc, deg
	ψ	stream function; $\psi_h = 0$, $\psi_c = 1$

```
ū
               total-pressure-loss coefficient
Subscripts:
               point on camber line where maximum camber line rise occurs
ad
               adiabatic
an
               annulus value
               arithmetic average at any plane
avg
               tip or casing at any plane
c
d
               downstream
               equivalent two-dimensional cascade
e
               hub at any plane
h
               immersion
j
               meridional direction
               polytropic
               suction surface
t
               tip at rotor leading-edge plane
               total when referring to blade element
               upstream
               with respect to axial displacement
               with respect to meridional displacement
               leading edge
2
               trailing edge
0.05, 0.95, 1.51, 1.57 instrumentation plane designations (fig. 5)
Superscripts:
               critical flow condition
```

relative to rotor

APPARATUS AND PROCEDURE

Test Rotor

The design of the rotor used in this test investigation is presented in reference 3 in which it is identified as Rotor 2D. The rotor was designed for a corrected weight flow per unit frontal area of 29.66 lbs/sec per square foot. With the selected rotor tip diameter of 36.5 inches and the hub-tip radius ratio of 0.50, the design corrected weight flow is 215.49 lbs/sec. The selection of a rotor tip solidity of 1.3, a diffusion factor of 0.45, zero inlet swirl, a rotor tip speed of 1400 ft/sec, and an axial velocity ratio of 0.91 permitted the calculation of the change in angular momentum across the rotor at the rotor tip. This change in angular momentum, with a suitable rotor total-pressure-loss coefficient derived from the NASA method of references 4 and 5, resulted in a design rotor total-pressure ratio of 1.76. The design total-pressure ratio was held constant radially. Because the loss correlation resulted in radially varying losses, a radial variation of the change in angular momentum was used in the design vector diagram calculations.

Double-circular-arc blade sections were used in the cascade projection* over the entire radial height of the blade. The same double-circular-arc blade sections were used for all Rotors 2 from the hub outward to approximately the 60% span location. However, for this rotor the portion of the blade outboard from the shroud also had a double-circular-arc section, resulting in a camber ratio of 0.65 for the tip element.

Tabulations of the blade design data appear in table 1. A view of a portion of the assembled rotor appears in figure l(a) and a close up of the tip section is presented in figure l(b).

In order to assess the quality of the blading, after manufacture, the blading was inspected using the contour layouts from six of the twelve manufacturing sections for six blades selected at random. A meridional view of the rotor appears in figure 2 and the inspected sections are identified by asterisks. At each manufacturing section the average of the six blades was obtained and was compared with the design intent. The results of the comparisons of the average blade sections with design intent appear in figures 3(a) through 3(f). These results indicate that most of the sections were more closed than the design intent in the trailing portion of the blade. Further investigation revealed that there was a manufacturing discrepency in the part-span shroud. The error in the shroud permitted the blade to open up more than design intent and partially compensated for the discrepency in the blade-trailing edge. Final conclusions

^{*}As described in reference 3, the cascade projection is obtained by viewing the intersection of a blade and an axisymmetric stream surface in the radial direction. The justification for the use of this projection is given in reference 6.

on the blade inspections are that generally the sections from the shroud outward were open about 0.3° and those from the shroud inward were closed about 0.3° from design intent.

The average running tip clearance at 100% speed was 0.042 inches.

Test Facility and Instrumentation

Performance tests of this rotor were made in General Electric's House Compressor Test Facility, in Lynn, Massachusetts. The general aspects of the test set-up are shown in figure 4 and described in detail in reference 7. The majority of the instrumentation was identical with that used in reference 7 and the locations are illustrated in figures 5 and 6. The difference in hub contour between Rotor 1 and Rotors 2 resulted in different radii for all of the instrumentation except the inlet pitot-static and casing boundary layer rakes. Photographs of fixed instrumentation used for Rotor 2D appear in figure 7. Photographs of the traverse probes and the hot-wire probes are presented in figure 8.

General Test Procedure

The following test sequence was followed in general during the testing of this rotor. With the throttle valve set to deliver approximately the design total-pressure ratio at 100% corrected speed, data were recorded from fixed instrumentation at 50%, 70%, 90%, 100% and 110% corrected speeds. (When only fixed instrumentation measurements are taken, the data readings are termed green readings). The test rotor was returned to 50% corrected speed and the throttle valve closed until the limit of stall-free operation was achieved. With the throttle re-set so that the vehicle operated as close to stall as feasible, blade-element data and a green reading were recorded. This procedure was repeated at 70, 90, 100, and 110 percent corrected speed to establish the limit of stall-free operation and to obtain blade element and green reading data early in the test. Blade element and green reading data were then recorded over the remaining range of stall-free operation up to the maximum facility flow capacity for 100%, 90% and 110% design speed.

Difficulties were encountered in determining the total-pressure ratio for green reading data at 50% and 70% corrected speeds. The level of the absolute total pressure at the rotor discharge was below the high accuracy range of the transducers for these conditions. The data recording system was modified for these speeds to record the discharge total pressures as differential pressures with the manifolded inlet total pressure as the reference. This method resulted in more reliable green reading data at 50% and 70% design speeds.

Blade element and green reading data were recorded over the remaining portion of the stall-free operating range up to the maximum facility flow capacity for 50 and 70 percent corrected speed.

Prior to the conclusion of the test the throttle valve was closed until the rotor was operating in stall where green reading and hot-wire data were recorded at each speed.

Testing in the Stall-Free Region

For all speeds the throttle positions at which data were recorded in the stall-free region of operation were generally selected to permit ease in defining the speed line and to document the peak efficiency. At low speeds this led to a relatively even spacing whereas at higher speeds the throttle positions were concentrated in the higher pressure ratio region where incidence variations occur.

At the rotor inlet traverse location, the static pressure wedge was set to zero flow direction and the cobra probe was allowed to seek its nulled position. At the rotor exit traverse location the static pressure wedge was manually rotated to the angle orientation established by the nulled position of the cobra probe; since stationary vane rows and struts were relatively far removed from this plane, circumferential variations of angle were presumed to be sufficiently small not to affect the pressure read by the wedge static probe. Probe immersion indicators and the probe aerodynamic parameters were connected to conventional X-Y plotting equipment. In general, continuous traverses were only recorded for the rotor exit flow angle; these were used to give an indication of the radial extent of the part span shroud wake. Recording of data from the traversing probes at the standard immersions was achieved by means of a digitized read-out on punched paper tape, as was also the case for the recording of data from fixed instrumentation.

Testing in the Stalled Region

Rotating stalls were encountered, on closing the throttle valve, at all speeds. The rotor was stalled twice at each speed, the limit of stall-free operation being established by closing the throttle valve slowly until distinct changes in the stress levels and performance were noted. For the first stall at each speed the three traverse hot-wire anemometer probes were immersed at the 10%, 50% and 70% immersions. In this way a knowledge of the radial extent of the rotating stall cells was gained. For the second stall the hot-wire anemometer probes were all set at the 10% immersion so that information was obtained from which the speed and number of rotating stall cells could be deduced. A green reading was recorded simultaneously with the hot-wire data with the rotor in stall.

RESULTS AND DISCUSSION

Overall Performance

The compressor map of the test rotor is shown in figure 9. The inlet total-temperature level was established as the arithmetic average of 24 inlet

temperatures measured in the low velocity region at the facility inlet screen (fig. 4). The rotor exit total-temperature and total-pressure ratio were established on the basis of fixed probe readings by a mass weighting routine, as follows. At each immersion, measurements from all circumferential locations were arithmetically averaged. The static pressure was assumed to vary linearly from hub to casing based on the measured average hub and casing values. With static pressure, total pressure, and total temperature known, static density and absolute velocity were computed at each immersion. The tangential velocity was obtained from the total-temperature rise and the Euler turbomachinery equation, and this, together with the absolute velocity and the design meridional streamline angle, gave the axial velocity. The discharge total-temperature and total-pressure ratio were then obtained from the following equations:

$$T = \frac{\sum_{j=1}^{5} T_{j} \rho_{j} V_{zj}^{A}_{j}}{\sum_{j=1}^{5} \rho_{j} V_{zj}^{A}_{j}}, \qquad (1)$$

$$\frac{P}{P_{in}} = \left\{ \sum_{j=1}^{5} \left[\left(\frac{P_{j}}{P_{in}} \right)^{\frac{\gamma-1}{\gamma}-1} \right] \rho_{j} V_{zj}^{A}_{j} + 1 \right\}$$

These quantities were used with the real gas properties of dry air to compute the rotor adiabatic and polytropic efficiencies.

The corrected weight flow was obtained from the calibrated venturi flow nozzles. For several points close to stall at 50% corrected speed the measurements of flow obtained from the venturi flow nozzles proved unreliable. A similar problem was encountered during the testing of Rotor 1B (ref. 7) and was resolved by establishing a relationship between the integrated flow from the rotor inlet traverse probe and the nozzle flow. Using this correlation and the integrated flow, the compressor flow was determined for all of the data at 50% corrected speed.

In reference 7, the performance at 100% corrected speed was compared with the design point by passing a constant throttle line through the design point and noting the intersection with the 100% corrected speed line. When this procedure is used on the Rotor 2D performance map (fig. 9) the resulting operating condition is too close to stall. For conditions at design speed, judged to have adequate stall margin for engine operation, a rotor total-pressure ratio of 1.677 and a rotor adiabatic efficiency of 0.854 were

actually achieved at a flow of 226.0 lbs/sec. The rotor was designed to deliver a total-pressure ratio of 1.76 and a rotor adiabatic efficiency of 0.837 at a flow of 215.49 lbs/sec. Peak rotor adiabatic efficiencies of 0.950, 0.958, 0.917, 0.875, and 0.814, were obtained at 50, 70, 90, 100, and 110 percent of design speed respectively. A completed listing of the overall performance data (green readings) appears in table 2.

Stall Performance

The throttle position representing the limit of stall-free performance of the rotor as the throttle is closed was recorded. With this information and performance data at throttle positions close to the stall throttle position it is possible to extrapolate each speed line on the compressor map to the limit of stall-free operation. The stall line determined in this manner is shown in figure 9. The overall performance measurements, recorded while the rotor was operating with stall present, appear as solid symbols in figure 9. The flow was quite unsteady for these readings leaving the absolute accuracy open to question, but indicating a notable decrease in performance.

Samples of the hot-wire anemometer data appear in figure 10. These are copies of Visicorder traces from the three anemometers. In figure 10(a) the anemometers are at immersions of 10%, 50% and 70%. A study of such traces gives an indication of the radial extent of the stall cells. In figure 10(b) all of the anemometers are at 10% immersion. The amplititude of the trace in figure 10(b) at the 111° position is greater than the correct level due to a data recording error. Under ideal conditions the trace in figure 10(a) at the 10% immersion would be identical to the trace in figure 10(b) at the 33° position since both are recorded at the same radial and circumferential location. Examination of these two traces reveals a general similarity but they are not identical because of slight variations in data recording techniques.

The number and speed of the rotating stall cells was calculated using the method described in reference 7 on traces similar to figure 10(b). These data and other stall performance information are presented in figure 10(c).

Blade-Element Performance

For presentation of the data from traverse probes located upstream and downstream of the rotor, a method of adjusting the data to obtain conditions at the blade edges was used. Knowing the measured total pressure, total temperature, static pressure and flow angle at each immersion and using the design meridional streamline angle, the meridional Mach number and all velocity components at each measurement plane may be calculated. Application of the condition of constant angular momentum along design streamlines yields the tangential velocity at each blade edge. It is assumed that the shape of each meridional stream tube, between a measurement plane and its

adjacent blade edge, remains fixed at the design shape for all data conditions. The meridional Mach number at a measurement plane may then be used to determine the meridional Mach number at the blade edge by use of the relationship shown in figure 11. This method is not strictly correct at the trailing edge where there may be an appreciable swirl velocity together with a change in radius between the edge and the measurement plane. Nevertheless, since the radius changes are not large, the method should be a very good approximation. With the tangential velocities and the meridional Mach numbers at the edges thus obtained, and with measured stagnation conditions assumed to be constant along the design streamlines, the velocities, Mach numbers, and all of their components may be determined at the blade edges. The constant physical quantities used in these computations at the measurement planes and at the edges are given in table 3.

In order to check out this procedure and to determine small differences due to calculation technique, design values of total pressure, total temperature, static pressure and flow angle were used in a simple calculation. Treating this information as though it were test data, the calculation routine was used to give design point blade element performance, yielding the data listed in table 4. Some indication of the small differences which can occur is indicated in table 4 by the leading edge and trailing edge check weight flow/nozzle weight flow ratios. The integrated flow at the upstream (plane 0.95) and downstream (plane 1.51) measurement planes is divided by the nozzle flow, which was set equal to the design flow for the check case. Table 5 is included to give a more complete description of the abbreviations used.

Complete listings of blade element data are given in table 6 and graphs of some blade element data, plotted as a function of incidence angle, are presented in figure 12.

Measurements of discharge stagnation temperature taken from the fixed instrumentation were judged to be more reliable than those from the cobra traversing probes. Efficiency, loss coefficient and loss parameter were therefore processed by separate computation, using fixed instrumentation stagnation temperatures and pressures in conjunction with the inlet relative Mach number obtained from the traverse probe data. The results of this computation are given as an addition in table 6 and loss coefficients obtained in this way are plotted in figure 12.

Examination of the blade-element data and the flow angle traverses in the rotor discharge plane revealed that the 50% immersion data were partially immersed in the wake of the part-span shroud. Similar results were observed and illustrated in figure 14 of reference 7 and figure 13 of reference 8. This effect can be seen in some of the unusually high values of loss coefficient for the third radial position on the blade-element data. Generally the influence of the shroud wake on the 50% immersion reading increased when the throttle position was close to stall or approaching maximum facility flow.

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Table 1. - Cascade Projection Data for Rotor 2D Blade Setting.

ψ	$\frac{r_1}{r_t}$	β1	i	~ ¹	κ's1 ^{-κ'} 1	tel ct
1.0	.9963	64.65	3,29	61.36	3.30	.0059
.9	. 9600	62.76	3.68	. 59.08	3.71	.0062
. 8	.9228	61.74	4.10	57.64	4.11	.0065
. 7	.8841	60.66	4.52	56.14	4.50	.0069
.6	.8435	59.64	4.94	54.70	4.97	.0072
.5	.8005	5 8.5 5	5.35	53.20	5.45	.0076
4	.7540	57.27	5.82	51.45	5.91	.0079
. 3	.7046	5 6.2 0	6.10	50.10	6.36	.0083
. 2	.6492	55.53	6.09	49.44	6.80	.0088
.1	.5850	56.18	5.90	50.28	7.23	.0093
0 .	.4995	61,18	5.70	55.48	7.56	.0100
	r_2	0.	δ°	1	0.1	t _{e2}
ψ	$\frac{r_2}{r_t}$	β'2	0	κ <mark>1</mark>	β <mark>†</mark> 2e	c _t
1.0	.9794	54.52	3.48	51.04	53.41	.0060
. 9	.9485	54,13	. 3.72	50.41	50.18	.0063
.8	.9157	52,77	3.92	48.8 5	47.77	.0066
. 7	.8815	50,72	4.15	46.57	45.09	.0070
.6	. 8454	47.78	4.57	43.21	41.71	.0074
. 5	.8070	44.05	5.05	39.00	37.76	.0078
. 4	.7675	39.12	5.73	33.39	32,78	.0082
. 3	.7257	33.36	6.71	26.65	27.15	.0086
. 2	.6824	26.32	8.21	18.11	19.68	.0091
. 1	.6378	18,34	10.70	7.64	8,52	. 0095
0	.5912	10.18	16.82	-6.64	-19.05	.0100
ψ	t _m	γ°	<u>a</u>	σ	φt	
Ψ	c t	,	ct		't	
1.0	.0350	56.19	.500	1,3063	10.33	
. 9	.0387	54.74	.500	1.3523	8.67	
. 8	.0426	53.24	. 500	1.4038	8.79	
. 7	.0466	51.35	. 500	1,4618	9.57	
. 6	.0510	48.95	. 500	1.5281	11.49	
. 5	.0556	46.10	. 500	1.6055	14.20	
. 4	.0604	42.42	. 500	1.6963	18.06	
.3	.0655	38.37	. 500	1.8044	23.45	
. 2	.0708	33.77	. 500	1.9382	31.33	
. 1	.0770	28,96	.500	2,1106	42.64	
0	.0850	24.42	. 500	2,3663	62.12	

Table 2. - Overall Performance based on Fixed Instrumentation

Rdg.*	Total press. ratio	Rotor adiab. eff.	Corrected weight flow	Rotor speed, percent design	Throttle valve setting	Operating mode	**Pressure measurement system
			lb/sec				
						6. 11 6	41
1	1.153	. 9640	124.35	50.02	11.7	Stall free Stall free	Abs. Abs.
2	1.322	. 9545	174.63	70.03	11.7 11.7	Stall free Stall free	Abs.
3	1,620	.9089	212,70	90.05	11.7	Stall free	Abs.
4	1.785	.8697	224.69 233.60	100.10 110.06	13.0	Stall free	Abs.
5 6m	1.837 1.174	.8063 .9055	99.4	50.03	5.0	Stall free	Abs.
6 T 7 T	1.174	. 8950	149.26	70.05	6.5	Stall free	Abs.
71 8T	1.671	.8910	201.26	90.05	9.4	Stall free	Abs.
9T	1.824	.8657	223.56	100.06	10.9	Stall free	Abs.
10T	1.943	.8118	232.99	110.05	11.5	Stall free	Abs.
111	1.369	.7775	225.67	99.98	50.0	Stall free	Abs.
12T	1.566	.8275	226.40	100.03	15.0	Stall free	Abs.
13 T	1.612	.8313	226.08	99.98	14.0	Stall free	Abs.
14 T	1.685	.8551	225.76	100.02	13.0	Stall free	Abs.
15 T	1.738	.8725	225.91	99.90	12.3	Stall free	Abs.
16T	1.782	.8715	225.24	100.06	11.7	Stall free	Abs.
17T	1.805	.8815	224.31	99.94	11.3	Stall free	Abs.
18T	1.318	.8318	215.50	90.02	50.0	Stall free	Abs.
19T	1.509	. 8980	216.05	90.03	14.0	Stall free	Abs.
20T	1.556	. 8996	214.88	90.04	13.0	Stall free	Abs.
21T	1.115	.9341	144.0	50.05	50.0	Stall free	Diff.
22T	1.124	. 9504	137.5	49.96	25.0	Stall free	Diff.
23T	1.140	. 9445	127.2	50.02	15.0	Stall free	Diff.
24 T	1.149	.9221	121.6	50.01	11.7	Stall free	Diff.
25T	1.157	.9253	114.8	50.04	9.0	Stall free	Diff.
26 T	1.164	.9138	107.4	50.01	7.0	Stall free	Diff.
27 T	1.215	.9006	187.52	70.06	50.0	Stall free	Diff.
28T	1.291	. 9471	179.75	69.97	15.0	Stall free	Diff.
29T	1.313	. 9683	174.55	69.96	12.3	Stall free	Diff.
30T	1.319	.9494	172.76	70.02	11.7	Stall free	Diff.
31T	1.346	. 9407	163.61	70.04	9.0	Stall free	Diff.
32T	1.355	. 9204	154.06	69.91	7.5	Stall free	Diff.
33T	1.621	.9180	212.89	90.02	11.0	Stall free	Abs.
34T	1.646	. 9174	209.41	90.00	11.0	Stall free	Abs.
35T	1.659	.9156	205.74	89.97	10.3	Stall free	Abs.
36T	1.440	. 7455	233.90	110.01	50.0	Stall free	Abs.
37 T	1.748	.7944	233.91	110.14	14.0	Stall free	Abs.
38T	1,829	. 8099	233.84	109.99	13.0	Stall free	Abs.
39T	1.889	.8138	233.13	110.03	12.3	Stall free	Abs.
40T	1.908	. 8128	233.00	109.95	12.0	Stall free	Abs.
41T	1.932	. 8131	232.06	110.04	11.7 11.7	Stall free Stall free	Abs. Abs.
42 43	1.934	.8136 .8711	232.45 225.66	110.08 100.06	11.7	Stall free Stall free	Abs.
43 44	1.784	.8766	224.31	100.14	11.3	Stall free	Abs.
45	1.807 1.824	.8741	223.54	100.14	11.0	Stall free	Abs.
46	1.687	.8544	225.52	100.17	13.0	Stall free	Abs.
47	1.623	.9123	212.06	90.12	11.7	Stall free	Abs.
48	1.381	.9617	183.87	75.06	11.7	Stall free	Abs.
49	1.325	.9579	172.71	70.10	11.7	Stall free	Abs.
50	1.226	.9655	146.17	60.07	11.7	Stall free	Abs.
51	1.154	.9611	122.83	50.06	11.7	Stall free	Abs.
52	1.883	.7699	220.26	110.11	10.7	Stalled	Abs.
53	1.740	.8018	207.55	100.09	10.1	Stalled	Abs.
54	1.587	.8046	184.22	90.10	8.4	Stalled	Abs.
55	1.277	. 7354	128.02	70.01	5.4	Stalled	Abs.
56	1.151	. 7877	91.03	50.04	4.1	Stalled	Abs.
				- · · · · ·			

^{*}The letter "T" following the reading number indicates Blade-Element Performance data were recorded.

^{**}Abs. - Instrumentation arranged to record absolute pressure at rotor inlet and exit.

Diff. - Instrumentation arranged to record difference between rotor inlet and exit pressures.

Table 3. - Constants Used in Data Analysis Methods
Columns list data in order of increasing immersion number

1.0906 1.0762 1.0709 1.0802 1.0582 . 9827 . 9720 . 9696 . 9745

1.363 1.494 1.650 1.849 2.136

> Frontal Area = 7.2660 Annulus Area = 5.4495

Radii are in inches. Areas are in square feet.

+ first and last values are casing and hub radii, respectively.

17.283 15.768 14.272 12.738 11.023

	$\left(\frac{\frac{w}{w^{\star}}}{\left(\frac{w}{w^{\star}}\right)_{u}}\right)$	$\frac{\left(\frac{w}{w}\right)}{\left(\frac{w}{w}\right)}$	$\stackrel{\overset{r}{r_{j}}}{\text{(Used for Diffusion Factor)}}$	of (Used for Diffusion Factor)
Plane 1.57	1.0067 .9206 .8285 .7593	17.836 17.166 15.817 14.501 13.198 11.864	07 .32 .42 .33 .33	
Plane 1.51	1.0320 .9483 .8661 .7831	17.838 17.148 15.770 14.391 13.012 11.634	68 .28 2.51 5.68 9.72	
Edge 2		17.887 17.201 15.768 14.354 12.921 11.516	-4.00 -0.50 3.00 7.00 13.40	50.18 45.03 36.17 23.45 5.78
Edge 1		18.182 17.392 15.759 14.180 12.456 10.494 9.116	-4.50 1.00 5.70 12.25 22.20	58.78 (62.55) 55.39 (60.14) 52.25 (57.96) 49.71 (56.28) 50.6 (57.88)
Plane 0.95	1,3108 1,1849 1,0814 1,0567 1,0967	18.323 17.473 15.733 14.023 12.191 10.023 8.550	-1.57 1.85 6.10 11.76 20.40	
Parameter	A j	 H +	ى ئى	κ'° (κ'°s)

Table 4. - Listing of Check Case for Blade Element Results Using Design Data.

	INLET AX. VELOCITY 690.864 693.508 680.879 651.214 529.312	EXIT AX. VELOCITY 575.793 562.776 564.862 599.334 661.221	AXIAL VEL.RATIO 0.833 0.811 0.811 1.259	
	INCET ABS MACH NO. 0.646 0.646 0.647 0.522	HACH ABS 0.657 0.792 0.792 0.796	EXIT REC 14806.VEC 7460.VEC 5050.060 3501.526 204.526 204.236 42.113 42.1133 44.929 45.535 46.535 46.535	600 470 400 9 0324 0408
4/14/1967	1 N L E T A B S V E L O C I T V 693.000 693.614 684.262 664.387 567.370	EXIT ABS VELOCITY 777.226 785.432 822.263 876.914 960.912	1 N L E T A R L 1 3 3 4 5 1 1 4 1 1 3 3 4 5 1 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	**************************************
A TS DATE	ADTOR SPD AT INLET 1334.214 1208.940 1087.808 955.553	MOTOR SPD AT EXIT 1319.562 1209.630 1101.156 991.225	MX 1 T ABS TANG VEL 550.500 5500 5500 5500 5500 5500 5500	ATION PRESSURE RATIO ADIABATIC EFF. POLYTROPIC EFF. NOZZLE WEIGHT FLOM F FLOW/NOZ. WEIGHT FLOW F FLOW/NOZ. WEIGHT FLOW
COMPRESSOR OUTPUT DAT MENT PERFORMANCE RESUL READING NUMBER 1	INLET REL VELOCITY 1503.455 1393.785 1285.123 1164.969 984.885	EXIT REL. VELOCITY 985.726 864.366 757.839 695.226	INLET ABS TANG. VEL 0. 0. 0. 0. 0. 1.22 1.220 1.215 1.215 1.203 1.193	IXED INSTRUMENTATION P A A A C. CHECK WEIGHT FLOWIN E. CHECK WEIGHT FLOWIN
S.A. ELEM	INLET REL MACH NO. 1.4012 1.2991 1.1964 1.0823 0.9055	EXIT REL. MACH NO. 0.8332 0.7355 0.6467 0.5993	CH1 0 4556 0 4987 0 5299 0 5299 0 3837 701, PRESS 1 760 1 760 1 760 1 760	FIXED INSTA T.E. CHECK
B NT NUMBER	INCID ANG SUCT. SURF 0.075 0.019 -0.003 -1.006	ANGLE ANGLE 8.401 10.784 16.196 25.165 39.710	NT. PRESS RIGE COMPT O. 339999 0.41049 0.41049 0.41049 0.4106 0.4106 0.4106 0.8116 0.8116 0.8116 0.8116 0.9174 9.174 0.9174	1.7600 1.8376 1.8500 1.0950 1.0950
104	INCID ANG MN.CMBR.LN 3.845 4.769 5.707 6.015	REL, DEV. ANG, T.E. 4,346 5,591 7,111	DIFFUSION FACTOR 0.471 0.552 0.554 0.448 ADIABATIC EFFICIENCY 0.8121 0.8121 0.8628	PRESSURE RATIO ADIAHATIC EFF. POLYTROPIC EFF. FFICTENT L.E. FFICTENT T.E.
	REL, INLET FLOW ANG. 62.625 60.159 57.957 58.725	FLOW ANG. 54.224 49.376 41.761 30.561 17.164		TRAVERSE PRESSURE RATIC TRAVERSE ADIAHATIC EFF TRAVERSE POLYTROPIC EFI FLOW COEFFICIENT L.E. FLOW COEFFICIENT T.E.
	P P P P P P P P P P P P P P P P P P P	P P P P P P P P P P P P P P P P P P P	P R A D S A	

Table 5. - Simulated Listing for Symbolic Identification of Column Headings.

INLET AX. VELOCITY	v_{z1}	EXIT AX. VELOCITY	V ₂₂	AXIAL Vel.ratio	$\frac{\frac{v_{22}}{z_{1}}}{v_{21}}$							
INLET ABS MACH NO.	rt z	EXIT ABS	m ²	EXIT REL	V [†] 2	ABS.EXIT FLOW ANG.	82					
INLET ABS	\rac{1}{\sqrt{1}}	EXIT ABS VELOCITY	V ₂	TANG. VEL	v*1	ABS.INCET FLOW AND.	$^{\beta}_{1}$	• • •	# # # 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3			
ROTOR SPO	.T	AOTOR SPD	$\mathbf{u_2}$	EXIT ABS TANG.VEL	V _{0.2}			PRESSURE RATIO ADIABATIC BFF. POLYTROPIC EFF	NOZZLE MEJGHT FLOM Mejght flom/Noz, Mejght flom Mejgwt flom/Noz, Wejght flom			
INLET REL VELOCITY	: <mark>-</mark>	EXIT REL. VELOCITY	V22	INLET ABS TANG, VEL	v ₆₁	TOT. TEMP RATIO	$\frac{r_{1.51}}{r_{0.95}}$		WEIGHT FLOW/N Weight flow/N		TOT, TEMP RATIO	$\frac{T_1.57}{T_0.05}$
MACH NO.	E ^T	MACH NO.		N H	౮	TOT, PHESS RATIO	$\frac{P_{1.51}}{P_{0.95}}$	FIXED INSTRUMENTATION	T.E. CHECK	RUMENTATION	TOT, PRESS RATIO	P _{1.57} P _{0.05}
SUCTO ANG	i la	REL TURN Angle	۵۵،	AISH CORFF	ပ ^a	POLVTROPIC EFFICIENCY	r. a		o u	FROM FIXED INST	LOSS COEFFICIENT	iз
INCID ANG	4	REL, DEV. Ang. T.E.	°	DIFFUSION	a	ADIABATIC EFFICIENCY	n ad	RATIO C EFF. IC EFF.	 	PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION	ADIABATIC EFFICIENCY	ad ad
REL.INLET FLOW ANG. B;	7	REL, EXIT FLOW ANG.	B.2					2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	FLOW COEPFICIENT	PARAME	TOT. PRESS LOSS PARAM	w.cosb. 20
RADIAL POSITION 1 2	o. 4. fV	RADIAL POSITION 1	।ਅਵਾਨ	RADIAL POSITION 1	: 10 4 TV	RADIAL POSITION	のちょた				RADIAL POSITION	(M M 4 W

Table 6. - Listing of Blade Element Performance

NASA - TASK I (ROTOR 2D) : N.A.S.A. COMPRESSOR OUTPUT DATA DIANE SIEMENT PEGFORMANTE DESILITS

	INLET AX.							EXIT AX.	VPLOCITY	277.210	299,429	268.081	314.679	341.004	AXIAL	VFL . RATIO	1.071	1.097	0.987	1.192	1.546									
	INLET ABS	MACH NO.	0.233	0,245	0.246	0,243	0.214	FXIT ABS	MACH NO.	0.350	0.351	0.352	0.387	0.439	EXIT REL	TANG. VEL	372.898	342.853	255.693	195,650	95.251	ABS.EXIT	FLOW ANG.	46.020	41,219	47.756	43,655	45.476	740 055 077	.39 .94799 .94051
1967	INLET ARS	VELOCITY	259,635	272,971	272,873	270,096	238,365	EXIT ABS	VELOCITY	399,675	398,083	399,009	436,651	493,052	INLET RAL	TANG, VFL	667,489;	604,816	544,216	478.050	402,750	ABS, INLFT	FLOW ANG.	0.			0	•	B M G	
RESULTS 6 DATE: 4/27/1967	ROTOR SPD	AT INLET	667,489	604,816	544,216	478,050	402,750	ROTOR SPD	AT EXIT	660,159	605,162	550.894	495,896	441.974	EXIT ABS	TANG. VEL	287,261	262,308	295,201	300.247	346,722								PRESSURE RATIO ADIABATIC EFF: POLYTROPIC FFF:	NOZZLF WEIGHT FLOW FLOW/NOZ, WEIGHT FLOW FLOW/NOZ, WEIGHT FLOW
	INLFT REL	VELACITY	716,207	663,563	608.794	549,075	467,971	EXIT HEL.	VELACITY	465,053	455,207	370,734	372,552	363,258	INLET ABS	TANG. VEL			.0	0	•0	TOT. TEMP	RATIO	1,065	1,053	1,052	1.049	1.050	UMENTATION P	NEIGHT FLOW/N WEIGHT FLOW/N
SE ELEMENT PERFORMANDE S READING NUMBER	INLET REL	MACH NO.	0.6428	0.5966	0.5479	0.4940	0.4207	EXIT REL.	MACH NO.	6.4073	0.4015	0.3273	0.3302	0,3233	CH1		0.4039	0,4555	(1,4815	0.4945	0.3737	TOT. PRESS	PATIO	1.170	1.168	1,159	1.168	1.179	FIXED INSTRUMENTATION	L.E. CHECK T.E. CHECK
BLADE NT NUMBER 6	INCID ANG	SUCT. SURF	6.255	5.572	5.524	4.816	3.405	REL. TURN	ANGLE	15.432	16.844	19.839	29.525	45.678	ST, PRESS	RISE COEFF	0.36161	0.43916	0.48299	0.53739	0.51417	POLYTROP1C	EFFICIENCY	0.7148	0.8673	0.8319	0.9244	0.9598	1,1689	
1104	INCID ANG	MN.CMBR.LN	10,025	10.322	11.234	11,386	10.685	REL, DEV,			α.	7.475	8,421	, à 2	DIFFUSION	FACTOR	6.497	0,446	0,539	0.471	0.405	ADIASATIC	EFFICIENCY	0.7084	0.8643	0.8283	6.9227	0,9588		TENT L.E. H
	REL . INLET	FLOW ANG.	68.805	55.712	63.484	61.096	61.285	REL. EXIT	FLOW ANG.	53,373	48,868	43.645	31.871	15.606															TRAVERSE PRESSURE RATIO TRAVERSE ADIABATIC EFF. THAVERSE POLYTROPIC EFF.	FLOW COEFFICE FLOW COEFFICE PERCENT DESIGN
	BADIAL	POSITION	। जना 	2	r	4	7	BADIAL	POSITION	-	2	₩	4	īv	RADIAL	PUSITION		2	٣	4	ī.	BADIAL	P0517104		2	٣	4	5		

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT, TEMP RATIO	
1	0.0475	0,7391	0.2170	1.172	1,063	
2	0.0180	0.8985	0.0819	1,174	1,052	
3	0.0159	0.9187	0.0724	1,168	1.049	
7	0.0030	0.9873	0.0132	1,174	1.047	
5	-0,0110	1,0344	-0.0487	1,183	1,048	

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (ROTOR 2D)

N.A.S.A. COMPRESSOR DUTPUT DATA

		104	JINI NUMBER 7	7 KEADING NUMBER	NUMBER 7	7 DATE 4/27/1967	1967		
KADIAL	REL. INLFT	INCIP ANG		INLET REL	INLFT REL	ROTOR SPD .	INLET ARS	INLET ABS	
POSITION	FICH ANG.	MN.CMBP.LN	SUCT.SURF	MACH NO.	VELOCITY	AT INLET	VELOCITY	MACH NO.	VELOCITY
,	082.40	7.440		0.9236	1021.861	934,634	413,109	0.373	
C ₁	64.607	6.217		(1.8570	945.452	846.878	420,330	0,381	
80	01.711	9.461	3.751	0.7855	866.347	762.024	412,162	0.374	
4	20.437	6.727	3.157	0.7092	782.098	669,377	404.489	0.367	395,279
r	and o.	9.238	1.958	0.6021	665,818	563,940	353.957	0.320	
न्दां∴स्भ	TIKE TENIT	REL. DEV.	REL. TUAN	EXIT REL.	EXIT REL.	ROTOR SPD	EXIT ABS	EXT ABS	EXIT AX.
POSITION	1 LUN A 200.	AMG. T.E.	ANGLE	MACH NO.	CITY	T EX I	VELOCITY	CNITAN	VE 00 137
* -1	52.521	2.341	13.699	6.5772	648.699	924.370	566.960	4	486 514
N	S.A. 5.4	3.602	14.975	0.5337	613,603	847.362	560.476	687	485 500
€:	-7.706	7.616	17.925	0.4364	500.807	771.374	558.197	6.4.0	361.000
4	54.574	F.124	27.863	0.4456	504.000	694,346	609,648	0.535	427.060
T,	25.429	10.049	44.016	0.4331	489.857	618.862	679.524	0.601	459,371
RADIAL		DIFFISION	ST, PRESS	CH1	INLET ABS	EXIT ARS	IN ET RE	EX T REI	14.54
POSITION		F ACTOR	RISE COFFF		TANG	TANG VE	TANG VE	TANG ABI	V#1 0 147
·		6.486	0,37974	0.4457		394,185	034.634	10 10 10 10 10 10 10 10 10 10 10 10 10 1	0.144.10
Λ:		0.408	0,44650	n.4852	. 0	386.876	846.878	460.486	
₩)		0.571	0.49925	6.5163	. 0	425.082	762.024	346.292	
4		6.507	0,55985	0.5332		471.004	669 377	242.046	100.0
r		0.444	0.55115	0.4260		488,625	563.940	150.237	1.402
YADIAL		ADIABATIC	POLYTROPIC	TOT, PRESS	TOT. TEXP		ABS. TALET	ARC EXIT	
POSITION		EFFICIENCY	EFF ICIENCY	01	RATIO		NA MO	SAA MOTE	
		0.7906	0.7997		1.119			44.11.88	
Λ.		9098.0	0.8667		1.106			43.652	
κ:		0.8329	0.8396		1.104		. 0	40.638	
4		6.9224	0.9257		1,099			45,323	
u		5446.0	0.9508		1.100		• 0	46.768	
	ddd dSedaesii	PPPSSURE BATIO	= 1.3582	FIXED INSTRUMENTATION		CITAG RAIISARG			
	THE TOTAL AND TAKE	THAT IT FEE							
	TANKERSE POLYTPOPIO EF	VIPCPIO EFF.	= 0.8687		< D.	POLYTROPIC FFF.	0.8995	2000	
	CLO. COEFFICIENT L.E.	SENT L.E.			i	NOZZLE WEIGHT FIO	0W = 14	•	
	PERCENT DESIGN SPEED	SPEED	= 950 = 70	T.E. CHECK METORY		FLOW/NOZ, WEIGHT FLOW Flow/NOZ WEIGHT Flow	19 11	0.08344	
							•	2010	

	ran	FARAMETERS DETERMINED FROM FIRED INSTRUMENTATION	ED FROM FIALD	INSTRUMENTALION		
RADIAL POSITION	TOT, PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT, TEMP RATIO	
	0,0399	0.7877	0,1789	1,367	1,119	
2	0.0221	0,8835	0.0997	1,361	1,104	
3	0.0222	0.8926	0,1013	1,347	1,100	
4	0.0071	0,9712	0.0307	1,356	1,094	
>	0.0050	0.9848	0,0222	1,372	1.096	

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK I (ROTOR 2D)

	N H H	VELOCITY	686.935	632,037	617,053	584.645	473,068	ENIT AX.	VELOCITY	506,735	526.924	545,596	539.260	559,986	AXIAL	VEL RATIO	0,835	0.833	0.836	0.922	1.184								
	TALET ABS	2		0.584	0.573	0.552	0.467	EXIT ABS	MACH		6	Ċ		9	FXI	TANG VEL	630,508	562.237	451.904	353,791	183,147	ABS, EXIT	FLOW ANG.	47.744	45.027	46.307	44.976	47.559	1.6710 0.8916 0.8986 1.28 0.994.9
/4967	TALET ARS	VFLOCITY	608.812	632,133	620.119	598,266	510.944	EXIT ABS	VELOCITY	754,401	744.988	746.877	765,175	840.476	INLET REL	TANG, VEL	1201.452	1088,643	979.545	860.470	724,933	ARS. INLET	FLOW ANG.		· c	•	•	• 0	330000000000000000000000000000000000000
JI DATA RESULTS 8 DATE - 4/27/4967	ROTOR SPD.	AT INLET	1201.452	1088,643	979.565	860,470	724,933	ROTOR SPD	AT EXIT	1188,258	1089.265	991,585	892,592	95.53	EXIT ABS	TANG, VEL	557,750	527,028	539,681	538,801	612,387								TION PRESSURE RATIC ADIABATIC EFF. POLYTROPIC FFF. NOZZLE WEIGHT FI FLOW/NOZ. WEIGHT FI FLOW/NOZ. WEIGHT FI 01
PERFORMANCE RESULT ING NUMBER 8 D	INLET RE	VFLOCITY	1346.900	1258.863	1159,351		886.	EXIT REL.	VELOCITY	809.677	770.298	686.138	648.347	604.090		TANG, VEL		0	•0	• 0	•0	TOT. TEMP	RATIO	1.214	1.189	1.181	1,163	1.163	INSTRUMENTATION A P P CHECK WEIGHT FLOW/N CHECK WEIGHT FLOW/N
N.A.S.A. COMPRE BLADE ELEMENT PE R 8 READING	INLET REL	MACH NO.	1.2366	1.1624	1.0712	0.9666	0.8111	EXIT REL.	MACH NO.	0.6907	0.6564	0.5880	0.5617	0.5280	CH1		0.5071	0.5613	0.6008	0.5086	.509	TOT. PRESS	PATIO	1.729	1.709	1.678	1.641	1.640	FixeD insTR
T NUMBE	INCID ANG	SUCT. SURF	0.049	-0.278	-0,169	-0,474	-1.007	REL. TURN	ANGLE	11.987	12.983	16.559	22.538	38.762	ST. PRESS	RISE CUEFF	0.40789	0.48898	0,55743	0.01158	0.61072	POLYTROPIC	EFF 101 ENCY	0.8071	0.8854	0.8905	0.9378	0.9376	1.0832 1.08724 1.0.8814 1.0.980 1.0.950
10d	INCID ANG	MN.CABR.LN	4.419	4.472	5.542	6.036	. 27	REL. DEV.	ANS. T.E.	•	1.349	5.064	9.818	12.331	DIFFUSION	FACTOR	0.550	0.528	. 55	0.522	4.8	ADIABATIC	EFFIG1ENCY	0.7917	0.3764	0.4822	0.7333	0.0331	•
	ARL.INLET	FLOW ANG.	24.149	508.65	242,50	55.806	55.873	MSL, FXII	FLOW A'16.	11.211	44,879	41.234	\$3.208	13.111															TRAVERSE PRESSURE RATIO TRAVERSE ADIARATIC EFF. TRAVERSE POLYTROPIC EFF FLOA COMPFICIENT L.E. FLOA COMPFICIENT T.E.
	RADIAL	P0511104	•	~	ĸ	4	ς.	RADIAL	POSITION		~	€	4	r	HADIAL	POSITION	-1	C.	۳	4	ĸ	HADIAL	POSITION	⊶ :	~	₩.	4	ī	

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

TOT. PRESS	ADIAE	ADIABATIC	ross	TOT. PRESS	TOT. TEMP
	EFFIC	CIENCY	COEFFICIENT	RATI 0	RATIO
6419	0.7	7778	0.2086	1.697	1,210
0224	9.0	8964	0.0978	1,710	1,185
0195	5.0	9141	0.0858	1,672	1,173
0,0067	0.9	0.9723	0.0297	1.638	1,156
0165	0.5	9475	0,0740	1.620	1,156

Table 6. - Listing of Blade Element Performance (continued).

WASA - TASK ! (ROTOR 2D)

	INLET AX.	VELOCITY	703,852	722,635	741.396	678.677	550.308	EX!T AX.	VELOCITY	591, R03	594.906	533,306	611.674	602.122	AXIAL	VEL.RATIO	0.841	0.826	0.750	0.901	1.094											
	INLET ABS	MACH NO.	0.656	0.674	0.668	0.647	0.548	EXIT	HACH			0.689		.0		TANG. VEL	678.860	630,357	486.144	371.024	223,430	ABS.FXIT	FLOW ANG.	47.307	44.177	49.101	45.454	47.649	1.824n 0.8657	3766 3766	18472	.98753
4727/1967	INLET ARS	۲	706,028	722.745	714.930	694.490	594.368	EXIT ABS	VELOCITY	873.764	832,362	815.018	874.744	905,232	INLET REL	TANG. VFL	1335.019	1209,669	1088.464	956,129	805.525	APS. INLET	FLOW ANG.	ċ	ċ	.0	٥.	٥.	4 11	# MO 13		•
<u>"</u>	POTOR SPD	AT INLET	1335,019	1209.669	1088,464	956,129	805,525	ROTOR SPE	AT EXIT	1320,358	1210,360	1101,821	991,823	883,974	FXIT ABS	TANG, VEL	641.498	580.003	615.677	650.799	640,544								PRESSURE RATIC ADIABATIC EFF.	POLYTPOPIC FFF	METGHT F	UZ, WEIGHT FL
SSOR OUTPUT D. RECRES!	INLET REL	7	1510,216	1409,135	1302,260	1141,736	1001,072	EXIT REL.	VFLOCITY	901,551	868.144	722,172	7,9,336	558,064	INLET ABS	TANG. VEL	0	0.	0	0	0	TOT. TEMP	RATIO	1.276	1.227	1,229	1.207	1.197		a z		WEIGHT FLOW/NUZ.
N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS 9 READING NUMBER 9 DA'	INCET REL	Z	1,4038	1.3149	1.2161	1.3016	0.9232	EXIT REL.	MACH NO.	n.7490	11.7344	0.6102	0.6190	0.5713	Ch1		0.4838	0.5500	0.5922	0.6624	0.5015	TOT. PRESS	PAT:0	1,920	1.890	1,619	1,839	1.755	FIXED INSTRUMENTATION			T. GIECK
NT NUMBER	INCID ANG	SUCT. SURF	-0.349	-0.993	-1.128	1.643	-2.220	REL. TUPN	ANGLE	13.281	12,583	14.481	23.392	35.302	ST. PRESS	RISE COFFE	0.36648	0.46022	0.53250	0.59031	45784.0	POLYTPUPIC	EFF101EMOY	0.7650	0.3901	0.3234	0.9272	0.3946	1,6523		•	100
104	0 NA C L D N F	MA CABR LX	3,421	3.757	4.582	. 32	5.160	REL. DEV.	-	-1.261	1.531	6.101	7.799	14.573	NCISHEIL	FACTOR	0.558	3,522	0.65.0	3,735	3.504	AUIABATIC	KONBIUI EBS	3.7437	3.4793	0.4145	3.7297	438F.C	H CITAS CARS SATIONS AND A MINISTER OF THE BEST OF THE		+ H	SPEED
	1 in 1 Ni - 1 in 1	FILL A VG.	62.241	59.147	36.357	54.637	15.60J	REL EXIT		. W. C	46.501	42,331	34.240	20.333															104 48541487 104 48541487	7.447=48E POLYTRO313 EFF	TABLE TO THE TABLE	PERCENT DESIGN
	3. T. A. D. C. D. C. A. D. D. C. A. D. D. C. A. D. D. C. D. D. C. D. D. D. C. D. D. C. D. D. D. D. D. C. D. D. D. D. D. C. D.	>C11150d	-	· ^	~	~ ~	5	7 4 11 1 4 ₹	2051113W		٠, ٥	· ~:	4	r	A A D I A i	NO111504		· ^	m	4	ž	3A1014	P051113V		0	∽	4	ır				

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

	25	FANATELENS DELENHINED INON LINED INSTRUMENTALION	מו נוערו ודעדו מי	NOT TWI WITH TO	
RADIAL POSITION	TOT. PRESS LOSS PARAM	AD1ABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT, TEMP RATIO
-	0,0575	0,7499	0,2387	1.845	1,255
2	0,0277	0.8754	0,1203	1.874	1,225
8	0,0309	6,98.0	0,1378	1.814	1,215
t	0.0094	0.9629	0.0408	1,823	1,194
5	0.0215	0.9278	0.0978	1.737	1,184

Table 6. -Listing of Blade Element Performance (continued).

NASA - TASK ! (ROTOR 2D) .

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N.A.S.A. COMPRESSOR NUTPUT NATA BLADE ELEMENT PERFORMANCE RESULTS

	INLET AX.	VFLOCITY	762.564	773.113	759,496	722.601	588.019	EXPT AX.	VFLOCITY	656.699	656.853	519.477	692.191	711.563	AXIAL	VFL. RATIO	0.861	0.850	0.684	0.958	1.210								
	INLET ABS							EXIT ARS	MACH NO.	0.794	0.768	0.721	0.840	606.0	FXIT REL	TANG. VEL	743.627	694,199	524.227	336.290	225.523	ABS.EXIT	FLOW ANG.	47.174	44.120	\$2.929	47.468	46.380	. 9430 . 8118 . 8285 . 99 . 9828 . 1059
1967	INLFT ARS	VELOCITY	764.922	773.231	763.270	739.437	635,098	EXIT ABS	VELOCITY	967,153	915.008	R62.188	1027,465	1045.240	INLET RFL.	TANG. VEL	1468.288	1330,425	1197.121	1051,576	885,937	ARS, INLET	FLOW ANG	٥.	٠.	.0	c.	ċ	2000
TE 4/27/				•			845,937	ROTOR SPD	AT EXIT	1452,164	1331,185	1211.811	1090.832	972.218	L ×	TANG.VEL	708.	636,986	687,583	754,542	746.694								ITION PRESSURE RATIC ADLYTROPIC FFF. NOZZLE WEIGHT FLOW I FLOW/NOZ. WEIGHT FLOW
ELEMENT PERFORMANCE RESULTS READING NUMBER 10 DA	INLET REL	VFLOCITY	1655,589	1538,804	1419.747	1285,526	1090.062	EXIT REL.	VEL OCTIV	993,148	955,721	738,520	774,237	765,454	INLET ABS	TANG. VEL	0	0	.0	0	0.	TOT. TEMP	RATIO	1,332	1.272	1.269	1.265	1.239	WEIGHT FLOW/
	INLET REL	MACH NO.	1.5509	1.4469	1.3352	1.2061	1.0100	FX17 REL.	MACH	0 R154	0.8017	0.6172	0.6632	n.6656	CH1		0.4229	3.4903	3,5268	0.5100	0.4074	TOT, PRESS	່ວ	800'2	000.	1.865	2.037	1.951	FIXED INSTRUMENTATION L.H. CHECK WEIGHT FLO T.E. CHECK WEIGHT FLO
BLADE Pojnt number 10	INCID ANG	SUCT. SURF	0.005	-0.301	-0.352	- 0.775	-1.453	Saut . IAA	T I SNA	14,002	13.256	12,347	29.593	38.841	ST. PRESS	RISE COFFE	0.2934K	0.38504	0.45122	0.48292	0.48502	POLYTROPIC	FEFFICIENCY	0,6954	0.8239	D.740H	0,8647	0.8935	1,9777 0,7726 0,7933 0,980 0,980
I (a	91V (1011	2 - 00		0.4	α	7.7.7	5.327	BEL DEV.	. u L 074	0.00	1.553	9.191	2.452		NULSERION	FACTOR.	35.	7.0.0	1.427	. 5. 11.00 11.00	0,165	A D I ? A T 1 ?	> 0.20世上で、19.40世	0.5646	9.3950	1.7259	3,4500	0.3830	SSURE CATTO = AddIIC EFF. = YTROPIC EFF. = 11-NT C.E. = SPEED
	THIND THE		10 1 C C	25.80	0.4	2 46 2 16 3 16 3 16 3 16	24.427	BE, CXIT			45.533	43.201	75.012	17.546															TRAJERS PRESSURE MATIO TRAJERSE ANIAMATIC EFF. TRAJERSE POUTROPIN EFF. FUNT CORFECTION U.E. FUNT CORFETCION U.E. PERCENT DESIGN SPEED.
	RADIAL	NO LET 1900		1 0		~ 4	r w	- 44 C: 44 O: 45	EC 11.000	, n	٠, ٠	. ~	0 41	ı v	2 2	20101202		10	. ~	- 4	٠.٠	4 1 1 4 9	14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		• •	~	4	τ	

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

	TOT. TEMP RATIO	1,299	1,249	1.240	1.225
	TOT, PRESS RATIO	1,949	1,870	1,932	1.957
	LOSS COEFFICIENT	0,2891	0.2181	0,1593	0.0887
INMINITER STREET	ADIABATIC EFFICIENCY	0.7020	0,7870	0.8619	0.9383
THE STATE OF THE S	TOT. PRESS LOSS PARAM	0.0702	0.0412	0,0388	0.0198
	RADIAL POSITION	- 0	3	, 4	

Table 6. - Listing of Blade Element Performance (continued).

NASA TASK 1 (HOTOR 2D)

N.A.S.A. COMPHESSOR NUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS BINT NUMBE? 11 READING NUMBER 11 DATE : 4/27/4

	IN FT AX.	VEI OCHTY	730,467	737.802	720.366	686.225	564.376	EXIT AX.	VELOCITY	800.082	723,041	654,126	864,623	900.044	AXIAL	VEL RATIO	1.695	0.980	906.0	1.260	1.596												
	INLET ABS	MACH NO.	0.685	0.691	0.678	0.656	0.564	EXTT ABS		0.754	•	•	0.892	•	EXIT REL	TANG, VEL	1 1082,534	945.250	754.995	523,476	270.448	** × 3	SNA MOIN	16.401	20.074	27.878	28.406	34.226	4911	775	A72	0.99031	0950
1967	INLET ARS	VELOCITY	732,726	737,914	723,945	702,243	609.542	×	VELOCITY	836,278	769,831	740.797	988.690	1110.578	INLET RFL	TANG. VFL	1334,035	1208,778	1067,642	955,424	904.931	TO INT	24 30 14			· c			u	u	, ,		n
DATE - 4/27/1967	ROTOR SPB	AT INLET	1334,035	1208.778	1087,662	955.424	804,931	ROTOR SPD	AT EXIT	1319,385	1209,468	1101,008	991.092	843,323	EXIT ABS	TANGIVEL	236,851	244,219	346,013	447,616	612,875								PRESSURE RATIC	DIABATIC EFF.	POLYTROPIC EFF.	FLOW/NOZ. WEIGHT FLOW	OZ. WEIGHT FLO
NUMBER 11	INLET REL	VELOCITY	1522,017	1416,213	1306,562	1185,723	1009,693	EXIT REL.	VELOCITY	1347.271	1190.094	999.537	1016.302	944.837	INLFT ABS	TANG. VEL	0	0	• 0	•0	• 0	TOT TEMP	RATIO	1.094	1.103	1.117	1.146	1.159		A	ā Þ	WEIGHT FLOW/N	
READING NUMBER	INCET MEL	MACH NO.	1,4222	1.3265	1.2233	1.1042	0.9334	EXIT REL.	MACH NO.	1.2151	1.0510	0.4831	1.9168	9.8829	CH1		0,1584	0.2188	1.2288	3.1609	-0.1188	TOT, PRESS	PATIO	1,295	1.292	1.257	1.496	1.573	FIXED INSTRUMENTATION			L.E. CHECK	CHECK
POINT NUMBER 11	INCID ANG	SUCT. SUAF	-1,253	-1,539	-1,477	-1,967	-2,915	REL, TURY	ANGLE	7.764	6.014	7,389	23.123	38,255	ST. PRESS	RISE CUEFF	0.09424	0.15895	0.18816	0.16586	0.01541	POLYTRIFIC	EFF 1C1EVCY	0.8735	0.7515	0.5914	O.d456	0.8801	1.3740		0.990	•	100
104	INCID ANS	Z - abro zz	2.517	3,211	4,233	4,503	4.354	PEL, DEV.	ANG. T.E.	3.353	7.557	12.324	7.742	10.329	PLFF JST 33	FAUTOR	9.172	0.222	0.316	0.251	0,193	STAPATIC	ADMILIES B	3.3220	3,7423	3.5783	3.4365	3.1724	PRESSUME RATIO =	• 1	u.	<u>ш</u>	
	7-111,67	FLUX ANG.	61.237	56.531	54.45	24. 713	32.454	AFL, FKII	FILLY A AG.	52.53	55.537	46.044	51.132	14.719															TRAVERSE POR	THE COURSE OF THE PARTY OF THE	1 1 1 1 1 1 1 1 1 1	FLOW CORFFICIENT	PERCENT DESIGN SPEED
	7 A l' 1 A L	P0511103		·×	~ 5	7	r	- A 1 1 A -	P.15111.51	+	:50	~	4	r	संकत्तिम्	POSITION	,-,	~	~	4	ኍ	741.147	POSITION	-	^	~;	4	ır					

PARAMETERS DETERMINED FROM FIXED INSTRIMENTATION

	TOT, TEMP RATIO	1.096 1.110 1.111 1.135 1.161
STRUMENTATION	TOT, PRESS RATIO	1,291 1,301 1,256 1,489 1,548
FROM FIXED IN	LOSS COEFFICIENT	0,0905 0,1480 0,2197 0,0849 0,2061
PAKAMETEKS DETERMINED FROM FIXED INSTRUMENTATION	ADIABATIC EFFICIENCY	0.7865 0.7111 0.6079 0.8925 0.8241
PAK	TOT. PRESS LOSS PARAM	0.0197 0.0301 0.0436 0.0196 0.0462
	RADIAL POSITION	2 6 3 3 5 1

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK I (ROTOR 2D)

N.A.S.A. COMPRESSOR DUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS

	IN FT AX.	VELOCITY	732,278	739.063	720.479	685.858	564,156	EXIT AY.	VELOCITY	698.125	664.850	551 597	727.434	804.930	AXIAL	0 t ± 4 0	0.953	0.900	0.766	1.061	1.427									
	INLET ABS	Q	0.686	0.692	0.677	0.656	0.563	ABA TEXT	MACH NO.	0.697	0.673	0.636	0.792	0.934	EXIT REL	TANG VE	917.193	810.051	609.612	466.523	247.262	- X	SNA MOTE	20.083	31,030	41,725	35,819	38,333	560 275 380	3638 3893
4/27/1967	INLET ARS	VELOCITY	734.542	739.176	724,059	701,838	609,325	EXIT ABS	VELOCITY	807,463	775.9n4	739.629	901,541	1043,916	INLET REL	TANG	1334,633	1209.320	1088,150	955,853	805,292	F3 141 204		•			0.	0.	0 = 1.5660 0.8275 0.8380 0.8380	S
Ŧ	ROTOR SPD .	AT INLFT	1334,633	1209.320	1088,150	955,853	805.292	ROTOR SPB	AT EXIT	1319,976	1210,010	1101,502	991,536	883,719	FX17 ABS	TANGVE	402,783	399,959	491,891	525,013	636,457								TION PRESSURE RATIO ADIABATIC EFF. POLYTROPIC EFF.	DZ. WEIGHT FLOW DZ. WEIGHT FLOW
ELEMENI MERFURMANGE RESULTS READING NUMBER 12 DA	INLET REL	VFLOCITY	1523,417	1417,334	1307,031	1185,846	1009,838	EXIT HEL.	VELACITY	1153.691	1047.971	822,631	848.782	863.610	INLFT ABS	TANG, VE	0	•0	0	.0	.0	ToT TEMB	RATIO	1.174	1,162	1,171	1,171	1,178	JMENTATION PE	HEIGHT FLOW/NOZ
	INLET REL	MACH NO.	1.4222	1.3277	1.2227	1,1077	0.9328	EXIT REL.	MACH NO.	6466.0	0.9086	0.7078	0,7636	0.7730	CH1		0.3444	6,3966	0.3943	0,3668	0.1140	TOT, PRESS	2AT10	1.562	1.556	1.450	1.619	1,638	FIXED INSTRUMENTATION	L.E. CHECK WEIGHT T.E. CHECK WEIGHT
BLADE INT NUMBER 12	INCID ANG	SUCT, SURF	-1.302	-1,571	1.469	-1.94]	-2,894	REL. TURN	ANGLE	8.524	7.947	8.631	21.666	37.910	ST. PRESS	RISE COEFF	0.23913	0.31024	0.33434	0.36998	0.20790	POLYTROPIC	EFFICIENCY	0.7960	0.8411	0.6723	0.6711	0.8651	1.5659 0.8006 0.8128 0.980	_
104	INCID ANG	MN.CMBR.LN	2.468	3.179	4.241	4.629	4.386	REL. DEV.	ANG. T.E.	2.543	5,593	11.690	9.223	11.296	DIFFUSION	FACTOR	0.339	0.355	0.485	0,389	0.299	ADIABATIC	EFF (CIENCY	0.7828	0.8309	0.6547	0.8620	0.8553	SSURE RATIO = ABATIC EFF. = YTROPIC EFF. =	
	REL.INLET	FLOW ANG.	61.248	28.569	26.491	m	54.946	MEL. EXIT	FLOW ANG.	52.723	50.623	47.850	52.673	17.076															TRAVERSE PRESSURE RATIO TRAVERSE ADIABATIC EFF TRAVERSE POLYTROPIC EFF FLOM COEFFICIENT L.E.	FLOW CHEFFICE
	WADIAL	PUSITION	•	2	m	4	ī.	BADIAL	POSITION	. 1	2	,	4	īv	MADIAL	PUSITION		ŒΝ	m	4	ľ	RADIAL	POSITION	-1	~;	m	4	ľ		

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

1,173	1,167	1,158	1,160	1,167
1,550	1,556	1,479	1,625	1.628
0,1606	0,1451	0,1957	0.0652	0,1280
0.770>	0.8047	0,7472	0.9292	0,8952
0.0357	0,0308	0.0398	0,0148	0.0286
1	2	3	7	5
	0.770 0.1606 1.550	0.770> 0.1606 1.550 0.8047 0.1451 1.556	0.770> 0.1606 1.550 0.8047 0.1451 1.556 0.7472 0.1957 1.479	1 0.0357 0.7705 0.1606 1.550 1.173 2 0.0308 0.8047 0.1451 1.556 1.167 3 0.0398 0.7472 0.1957 1.479 1.158 4 0.0148 0.9292 0.0652 1.625 1.160

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK ! (ROTOR 2D)

	INLET AX. VELOCITY VSS.0850 VSS.273 V48.271 678.661	EXIT AX. VELOCITY 684.408 669.453 595.060 708.313	AXIAL VFL.RATIO 0.903 0.906 0.773 1.044 1.413		
	TNLET ABS MACH NO. 0.693 0.675 0.648	EXTT ABS HACH NO. 0.695 0.695 0.699 0.790	FX1T REL TANG. VEL TANG. 284 770.951 569.004 440.101	ABS. EX17 FLOW ANG. 32.324 33.224 43.783 37.878 39.993	6120 8313 8423 8423 985 985 00925
4/27/1967	IALET ARS VFLOCITY 736.119 739.386 721.840 694.473 598.430	EXIT ARS VELOCITY 811.324 800.292 769.371 901.571	IALET RFL TANG. VFL 1333.995 1208.741 1087.630 955.396	APS. INLPT FLOW ANS. 00. 00.	
SATE	ROTOR SPD 1333.995 1208.741 1087.630 955.396	ROTOR SPC AT EXIT 1319.345 1209.432 1100.976 991.062 883.296	EXIT ABS TANG, VEL 433.061 438.491 531.972 550.961		SURE RATI BATIC EFF TROPIC EF LE WEIGHT F WEIGHT F
COMPRESSOR OUTPUT DATA ENT PERFORMANCE RESULTS EADING NUMBER 13 DA	INLET REL VELOCITY 1573.619 1416.950 1305.370 1181.133	EXIT REL. VELOCITY 1120,806 1021,061 795,426 838,427 836,007	INLET ABS TANG. VEL 0.00.00.00.00.00.00.00.00.00.00.00.00.0	101. TEMP RATIO 1.192 1.176 1.178 1.178	33
Ε. Α Ε. Ε. Α	INLET REL MACH NO. 1.4233 1.3272 1.2208 1,1024 0.9262	EXIT REL. HACH NO. 0.9603 0.8820 0.6818 0.7347	CH1 0.3770 0.4233 0.4235 0.4139	TOT. PRESS RATIO 1.622 1.627 1.520 1.654	FIXED INSTRUMENTATION
N.A.S BLADE INT NUMBER 13	INCID ANG SUCT. SURF 11.306 -1.590 -1.401 -1.664	REL. TURN ANGLE 6.860 9.519 10.848 22.758	ST. PRESS RISE COEFF 0.28496 0.38496 0.39708 0.39708	POLYTROPIC EFFICIENCY 0.788A 0.8575 0.6990 0.8801	1,6191 0,8063 1,0191 1,0190 1,0190 1,050
104	INCID ANG MN.CMBR.LN 2.404 3.160 4.309 4.902 4.958	REL. DEV. ANG. T.E. 2.144 7.4.301 9.541 8.404 10.365	01FFUSION FACTOR 0.368 0.383 0.515 0.418	ADIAPATIC FFFICIENCY 0.7737 0.8473 0.6807 0.8713	C • ii.
	RFL, IMLET FLUW ANG. 61.184 54.550 56.559 54.612 55.559	RFL, EXIT FLOW ANG, 52.324 49.031 45.711 31.854			TRAVERSE PRESSURE RA TRAVERSE ADIAHATIO E TRAVERSE POLYTOPPIO FLOW COEFFICIENT L.E FLOW COEFFICIENT T.E PERCENT DESIGN SPEED
	MADIAL POSITION 1 2 3 5 5	RADIAL PUSITION 2 3 3 5 5	RADIAL POSITICN 2 2 3 3	RADIAL POSITICN 1 2 3 4 4	

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TOT, TEMP RATIO	1.188 1.178 1.171 1.167	
TOT. PRESS RATIO	1,593 1,620 1,543 1,659	
LOSS COEFFICIENT	0, 1804 0, 1336 0, 1886 0, 0648 0, 1521	
ADIABATIC EFFICIENCY	0,7579 0,8300 0,7725 0,9325 0,8813	
TOT. PRESS LOSS PARAM	0.0404 0.0293 0.0399 0.0149 0.0342	
RADIAL POSITION	2 6 7 3 5 1	

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK ! (ROTOR 2D)

N,A,S,A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS INT NUMBER 14 PARADING NUMBER 14 DATE: 4/27/1967

	INLET AX.	VELOCITY	727,253	736.722	719.307	665,436	560.548	EXIT AX.	VELOCITY	670.422	642,455	590,875	671.144	712.740	AXIAL	VEL RATIO	0.922	0.872	0.766	0.979	1.272												
	INLET ABS	MACH NO.	0.681	0.690	0.676	0.655	0.559		MACH NO.	669.0	0.689	0.674	0.770	0.866	EXIT REL	TANG. VEL	845.059	727.480	533,753	418.753	228,460	ARC EXIT	FLOW AND	35,306	36.902	45.859	40.474	42,590	850	654	9	0932	
4/27/1967	INLET ABS	VELOCITY	729.502	736.834	722.881	701.406	605.428	EXIT ABS	VELOCITY	822,852	803,430	791.525	886,111	982.893	INLET RFL	TANG. VEL	1334.500	1209,199	1088.041	955,758	805.212	ABS. INI ET				•	•	٥.	a (_	LOW # 225.7		
TE ,	ROTOR SPD	AT INLET	1334,500	1209.199	1088.041	955,758	805,212							883.631		TANG.VEL	474.785	482,410	547,640	572,685	655,171								PRESSURE RATIO	SLYTROPIC EFF	DZZLF WEIGHT	FLOW/NOZ. WEIGHT FLOI	
BLADE ELEMENT PERFORMANCE RESULTS 14 READING NUMBER 14 DA	INLET REL	VELOCITY	1520,876	1416.011	1306.289	1185.514	1007.427	EXIT REL.	VELOCITY	1079,717	970,570	747,586	795,348	767,479	INLET ABS	TANG, VEL	0	•	•	0	• 0	TOT. TEMP	•	1,213	1,193	1.206	1.189	1.189	MENTATION P	ŧ ū.) Z	WEIGHT FLOW/NO	
E ELEMENT PEF READING	INCET REL	MACH NO.	1.4193	1.3255	1.2219	1.1063	0.9302	EXIT REL.	MACH NO.	0.9172	0.8319	0.6538	n, 6912	0.6766	CH1		0.4101	0.4697	0.4899	0.4977	0.3023	TOT. PRESS	AT10	1.701	1.707	1.635	1.724	1.699	FIXED INSTRUMENTATION) () ()	T.E. CHECK	
NT NUMBER	INCID ANG	SUCT. SURF	-1.139	-1,492	-1,429	-1.927	-2.724	REL. TURN	ANGLE	9,838	10.096	12,436	22,392	37,384	ST. PRESS	RISE COFFF	0,29669	0.37912	0.42663	0.47981	0,38441	POLYTROPIC	EFF 1C1 ENCY	6,7853	0,8665	0.7501	0.9005	0.8787		0.8320		_	
104	INCID ANG	MN CMBR.LN	2.631	3.258	4,281	4.643	4.556	PEL, DEV.	ANG. T.E.	1.394	3.521	7.926	8.512	11.993	DIFFUSION	FACTOR	0.404	0.429	0.545	0.462		ADIABATIC	FFFICIENCY	0,7687	0.8560	0.7323	0.8926	0,8693	PRESSURE RATIO =	-	ENT L.E.		
	RFL, INLET	FLUM ANG.	61,411	58.64E	56.531	54.353	55.156	RFL. FXIT	FLOW ANG.	51.574	48.551	44.096	31.962	17.773															TRAVERSE PRES	TRAVERSE POLYTROPIC EFF	FLOW CORFFICE	PERCENT DESIGN	
	RADIAL	POSITION	, , 1	~	m	4	ľΩ	RADIAL	POSITION		~	m	4	Z.	HADIAL	PUSITION		~	m	4	εc	RADIAL	POSITION	w-1	~	m	4	īv					

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

TOT, TEMP RATIO	1,207	1,192	1,187	1,176	1,175
TOT. PRESS RATIO	1,669	1,701	1.649	1,721	1,685
LOSS COEFFICIENT	0,1939	0,1220	0,1596	0.0462	0,1015
ADIABATIC EFFICIENCY	0,7601	0.8548	0.8226	0,9539	0,9207
TOT. PRESS LOSS PARAM	0.0442	0.0270	0.0347	0.0106	0.0226
RADIAL POSITION	-	2	m	4	2

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK I (RNTOR 2D)

	INLET AX. VELOCHTV 725.409 735.812 742.294 681.380	FX - X - X - X - X - X - X - X - X - X -	AXIAL CFL.RATIO 0.891 0.346 0.773 1.965	
	INLET ABS MACH NO. 0.679 0.670 0.670 0.651	A A D C A A D C A A D C A A D C A A D C C D C C D C C C C	AXIT REL 1ANG. VEL 1902. 620 584.827 398.905 238.475 238.741 100.121 100.121 100.121 100.121 100.121 100.121	1.7%#0 0.8725 0.8%21 0.9%36 1.00432
4/27/1967	INLET ARS VELOCITY 727.652 735.924 715.834 697.256	EXIT A95 VELOCITY 834.320 813.500 805.609 888.106	INLFT REL TANG. VFL 1332.907 1207.756 1085.743 954.617 804.251 APS.INLFT FLOW ANG. 0.	и и и и и и и и и и и и и и и и и и и
S ATE	ROTOR SPD AT INLET 1332-907 1207.756 1086.743 954.617 804.251	POTOR SPD AT EXIT 1318.269 1208.445 1100.078 990.254 882.576	EXIT ARS TANG.VFL 525.649 523.618 591.349 648.841	10N PRESSURF RATIC ADIABATIC EFF. POLYTROPIC FFF. NOZZLE WEIGHT FIOW FLOW/NOZ. WEIGHT FLOW
S.A. COMPRESSOR OUTPUT DATA ELEMENT PERFORMANCE RESULTS READING NUMBER 15 DA	INLET REL VELOCITY 1518.591 1414.305 1301.317 1182.142	EXIT REL. VELNCITY 1023,733 925,524 752,569 773,409	INLET ABS TANG. VEL 0.00.00.00.00.00.00.00.00.00.00.00.00.0	33
N.A.S.A. COMPRESSOR OUTPUT DATA LADE ELEMENT PERFORMANCE RESULT 15 READING NUMBER 15 D	12LET REL MACH NO. 1.4179 1.3227 1.2177 1.1037	EXIT REL. HACH NO. 0.4631 0.7890 0.6399 0.6702	CH1 0.4425 0.5001 0.5256 0.5371 0.3938 TOT. PHESS 1.766 1.768 1.777 1.716	FIXED INSTRUMENTATION L.E. CHECK WEIGHT FLO T.E. CHECK WEIGHT FLO
N.A.S BLADE NT NUMBER 15	INCID ANG SUCT.SUPF -1.106 -1.491 -1.202 -1.798 -2.374	PEL, TURN ANGLE 10.653 10.952 13.799 23.243	ST. PRESS 81SE COEFF 0.32627 0.40914 0.46310 0.52081 0.47654 POLYTROPIC FFICIENCY 0.6667 0.9103 0.8792	1.7526 0.8232 0.8366 0.950
100	INCID ANG MN.CMBP.LN 2.564 3.259 4.568 4.772 4.772	PFL. DEV. 0.425 0.425 0.425 0.425 0.425 0.425 0.489 0.480 0.489 0.489 0.480 0.480 0.480 0.480 0.480 0.480 0.480 0.480 0.	FACTOR 6.450 N FELTOR 6.450 N	PPESSURE BATTO = ANIMARATIC EFF. = POLYTROFIC EFF. = FIGIENT L.E. = FIGIENT T.E. = SIGN SPEED
	######################################	FUGS AND		TRAVERSE PRESSURE PATTO TRAVERSE ANDABATO EFF TRAVERSE POLYTROFIC EFF FLOW COEFFICIENT L.E. FLOW CHEFFICIENT T.E. PERCENT DESIGN SPEED
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 TOT. PRESS
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 0.7634
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 1.735
 1.223

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 0.1130
 1.765
 1.202

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 0.8500
 0.1417
 1.715
 1.196

 0.0060
 0.9751
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 1.767
 1.181

 0.0131
 0.9537
 0.0592
 1.699
 1.171

RADIAL POSITION

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK 1 (RNTOR 2D)

N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS NT NUMBER 16 NEADING NUMBER 16 DATE 4/27/1967

	INLET AX.	VELACITY	715.395	730.285	746.687	683,342	596.091	FXIT AX.	VFLACITY	624, R97	609.419	536.980	637.156	626.506	AXIAL	VFL.RATIO	0.873	0.834	0.749	0.932	1.127										
	INLET ABS	MACH NO.	0.668	0.683	0.673	0.653	0.554	FXIT ARS	MACH NO.	0.710	0.696	0.680	0.759	0.797	FXIT REL	' TANG.VEL	749.528	662.530	505,383	390,339	233,498	ABS, EXIT	FLOW ANG.	42.410	41.952	48.002	43.349	46.075	A20	\$ \$.9841B .99563
1967	INLET ARS	VELOCITY	717.607	730,397	720.249	699.264	600.614	EXII ARS	VELOCITY	847.478	819,456	803.024	879.6R5	915.359	INLET RFL	TANG. VFL	1334,990	1209,643	1088.441	956.108	805.547	P.S.	FLOW ANG.		9	ċ	0.			H H	H H
DATE 4/27/1967	POTOR SPB.	AT INLFT	1334,990	1209.643	1088,441	956,108	805.507	ROTOR SPD	AT EXIT	1320,329	1210.334	1101.797	991,801	883,955	FXIT ARS	TANG, VFL	570,841	547,804	506,414	601.462	650,457								PRESSURE RATICADIABATIC EFF.	JOZZLE WEIGHT	r FLOWANDZ, WEIGHT FLOW r FLOWANDZ, WEIGHT FLOW
NUMBER 16	INLET REL	VELOCITY	1515,638	1413,052	1305,167	1184,531	1004,778	EYIT REL.	VELOCITY	976.831	900,203	737,937	751.301	685.061	INLET ABS	TANG, VEL		0	•	0	.0	TOT. TEMP	RATIO	1,251	1.218	1.222	1.204	1.194	UMENTATION P	n 2	WEIGHT FLOW/N
NUMBER 16 READING NUMBER	INLET REL	MACH NO.	1,4113	1.3216	1,2202	1.1659	0.9272	EXIT REL.	HOW HOW	0.8181	0.7644	0.5248	3.6483	0.5965	C+1		1,4627	0,5259	0.5654	0.5746	0.4601	TOT, PRESS	RATIO	1.438	1,627	1.761	1.409	1.731	FIXED INSTRUMENTATION		L.E. CHECK
POINT NUMBER 16	INCID ANG	SUCT, SUPF	-0.736	-1,260	-1,323	-1,834	-2,500	REL. TURN	ANGLE	11.633	11.489	13,373	22.953	34.940	ST, PRESS	RISE COEFF	0.34570	0.43495	0.50383	0.55994	0.54339	POLYTRUPIC	EFFICIENCY	0,7782	0.8729	0.8061	0,9135	0.8879	= 1.7989 = 0.8297		= n.950 = 100
10d	TACIP ANG	MY. CYBR. LN	3.734	764.8	4.387	4.736	4.780	REL. Drv.	4 . F . 6 . 4 . F .	() () () () () ()	2.761	7.094	R 40.8	14.460	PIFFUSION	FACTOR	0.493	£67.9	6.574	16 TO 16 TO 1	0.477	APIAFATIC	FFF1C1ENCY	0.7565	0.8616	0.7961	5506*1	5à2±°1	6 • I	L	
	THINI LAN	FI ON ARE.	61.814	ייבר המני אני	54.43	24.446	55.450	REL. FXIT	F1 (14) A %.C	50.181	4.7 3.6	43.264	54.443	20.440								~							TRAVERSE PPE TRAVERSE ADI	TRAVERSE POLYTROPIC E FLOW COEFFICIENT LIE:	FLOW COEFFICIENT 1.E. PERCENT DESIGN SPEED
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PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

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RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT, TEMP RATIO
1	0.0504	0.7620	0.2147	1,789	1,237
2	0.0243	0.8831	0,1072	1.820	1,211
3	0.0300	0.8608	0.1362	1,765	1,205
4	0.0064	0.9740	0,0276	1,800	1,188
2	0.0223	0.9231	0,1018	1,716	1,181

Table 6. - Listing of Blade Element Performance (continued).
NASA - TASK 1 (ROTOR 2D)

	1NLFT AX. VPLOC11Y 746.927 730.167 708.770 669.948 849.361	FX:1 AX.	AXIAL VFL.RATIO 0.857 0.759 0.939 1.118	
	INLET ABS MACH NO. 0.671 0.683 0.666 0.540	FX11 ABS MACH NO. 0.703 0.701 0.689 0.762	# # # # # # # # # # # # # # # # # # #	1,805n 0,8415 0,8410 4,31 0,98538 0,98531
4727/1967	1 IALET ARS VFLOCITY 719.144 730.278 712.292 685.558 593.345	EXIT ARS VELNCITY R66.761 R76.261 813.051 882.012	1 A N B T A A B A B A B A B A B A B A B A B A	
S A T E	ROTOR SPD AT INLFT 1333.451 1208.249 1087.186 955.006	AT EXIT 1318.807 1208.939 1100.527 990.658	EXIT ARS TANG.VEL 609.784 562.209 617.542 613.689 652.439	10N PRESSURE RATIC ADIABATIC EFF. POLYTROPIC FFF. NOZZLE WEIGHT FLOW FLOW/NOZ. WEIGHT FLOW
N.A.S.A. COMPRESSOR OUTPUT DATA LADE ELEMENT PERFORMANCE RESULTS 17 DA	INLFT REL VFLNCITY 1515.012 1411.797 1299.744 1175.596	EXIT REL. VELNCITY 919.230 885.938 731.423 737.182	INLET ARS TANG. VEL 0. 0. 0. 0. 1.268 1.223 1.223 1.223 1.225	UHENTATION PARTICULARION PROPERTIES AND PARTICULARION PROPERTY PLONGY NATIONAL PROPERTY PROPE
S.A. COMPRES E ELEMENT PER PEADING	INLET REL MACH NO. 1.4127 1.3205 1.2156 1.0969	FXIT REL. MACH NO. 0.7835 0.7515 0.5202 1.5367	CH1 CH2 CH2 CH3 CH3 CH3 CH3 CH3 CH3 CH3 CH3	FIXED INSTRUMENTATION L.E. CHECK WEIGHT FLO T.E. CHECK WEIGHT FLO
B NUMBER	INCID ANG SUCT. SUPF -0.515 -1.285 -1.062 -1.336 -2.205	PEL. TURN 12.650 11.966 14.482 24.006 35.096	ST. PRESS HISE CCFFF 0.35724 0.56994 0.56499 0.56499 POLYTRUPIC EFFICIENCY 0.8823 0.8823 0.8164 0.88664	1.H264 0.6299 0.H437 0.950
FNICA	T N C C C C B D A A A A A A A A A A A A A A A A A A	DEL. DEV. ANG. 1.6. 1.794 6.246 7.497	PIFFUSION C. 527 C. 580 C. 580 C. 580 O. 487 AULAPATIC FFI DIFNOY C. 7423 C. 7	PRESSURE DATIONS ADILMATIC EFF. SPOLYTROPIC FFF. SPICIFIC FFF. SPICIN L.S. SPICIN SPEED
	941. JNLFT +101. ANG. 57. ASS 56. 898 54. 950 57. 655	FE. FX1T FLOV ANG. 40.046 46.887 40.416 50.943		TRAVERSE ADTARATIC EFF. THAVERSE ADTARATIC EFF. THAVERSE POLYTROPIC FFF. ELDW COEFFICIENT L.S. ELDW COFFFICIENT L.S. ELDW COFFFICIENT T.E.
	KADIAL PUSITION 2 2 8 8	AADIAL FOSITION 1 2 3 3 4 5	A A D I A L L L L L L L L L L L L L L L L L L	

INSTRUMENTATION
FIXED
FROM
DETERMINED
PARAMETERS

TOT. TEMP RATIO	1,245	1,217	1,209	1,190	1,173
TOT. PRESS RATIO	1,823	1,851	1,792	1.814	1,127
LOSS COEFFICIENT	0.2182	0,1052	0.1304	0.0278	0.0321
ADIABATIC EFFICIENCY	0.7639	0.8877	0.8695	0,9744	0,9753
TOT. PRESS LOSS PARAM	0.0524	0.0241	0.0292	0,0065	0.0070
RADIAL POSITION	1	2	3	~7	5

Table 6. - Listing of Blade Element Performance (continued), NASA - 1ASK 1 (ROTOR 2D)

N.A.S.A. COMPRESSOR NUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS POINT NUMBER 18 READING NUMBER 18 DATE. 4/27/1967

	S INLET AX.						925, A30							866.775	AXIAL	. >					1.648			•								
	INLET AB	MACH NO	0.630	0.636	0.627	0.609	0.523	EXIT ABS	NATION	0.690	0.643	0.605	0.792	0.957	EXIT RFL	TANG. VFL	979.453	847.436	692.980	491.308	244,487	ABS, FXIT	FLOW ANG	15.847	20,036	25.961	27,254	32,435	1180	1318	0.8382	0.99197
4/27/1967	INLET ARS	VELOCITY	678.312	683,340	673.626	655,142	567.931	EXIT ABS		765,093	719,507	682.2N7	880.922	1047.545	INLET REL	TANG. VFL	1201.0041	1088.318	979.272	A 60.243	724.747	ARS, INLET	FLOW AND			.0	9.	• 0	e: e-f	H .	11 /	1 H H 8
υź	ROTOR SPD	AT INLET	1201.094	1088,318	979.272	860,213	724.717	ROTOR SPB	AT FXIT	1187,903	10AB.940	991.289	892,326	795.296	EXIT ARS	TANG. VEL	208.450	246.504	298.308	401.018	550.809								PRESSURF RATIC	ADIABATIC FFF.		FLOW/NOZ. WEIGHT FLOW FLOW/NOZ. WEIGHT FLOW
NUMBER 18	INLET REL	VELOCITY	1379,396	1285.064	1188.590	1081,297	920,739	EXIT REL.	VFLACITY	1225,253	10R0.104	925.549	925.522	923,966	INLET ABS	TANG. VEL	0	•	•	•	0	-										FLOW
BLADE ELEGEN! FERFURANCE RESULTS 3 18 MEADING NUMBER 18 DA	INCET REC	MACH NO.	1.2802	1.1958	1,1061	1.0044	0.8474	EXIT REL.	PACH NO.	1.1046	1.9647	0.4204	0.6324	G. H445	CH1		0.1086	0.2235	0.2316	0.2180	-0.1326	TUT. PRESS	RATIO .	1.248	1.250	1.208	4.415	1.492	FIXED INSTRUMENTATION			T.E. CHECK WEIGHT
NT NUMBER	INCID ANG	SUCT. SUPF	-1.930	-2.260	-2.351	2.940	-3.843	REL. TURM	ANGLE	7.481	6.622	0.00.7	21.085	36.245	ST, PRESS	RISE COFFF	0.16936	0.17227	0.19925	0.22259	-0.00507	POLYTROPIC	EFF 1CIENCY	6.8635	C.762A	C.5%.5	0.8869	6.8839				0.450
104	INCID ANG	MY. CHBE. LN	1.840	2.490	3.259	3.530	3.437	PEL. DEV.	ANG. T.E.	5.059	6.228	12.349	•	26.5	PIFFUSICN	FACTOP	(.167	0.224	850.0	6.246	0.143	ADIABATIC	FFFICIERCY	(i. c 6 4 4	0.7549	6,5736	0.981%	2772	PPESSUPE PAT'0 =	AHATIC EFF. =		
	KFL, INLET	FLOW ANG.	964.86	57. AFC	56.409	53.340	54.037	PEL. FXIT	Fills And.	53,139	53.058	2 £ 7 . 4 4	32.256	15.752															TRAVERSE PPE	TRAVERSE APIAHATIC EFF.	FLOS CORFETCIANT LES	FLOW COPFFICIENT T.E. PERCENT DESIGN SPEED
	RADIAL	POSITION	-	~	m	4	r	KADIAL	POSITION	-	~	™	4	ſΛ	HADIAL	POSITION	-1	α,	m	4	r	RADIAL	POSITION	. .	~	≈ 0	4	ır				

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

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TOT. TEMP RATIO	1,079	1,093	1.090	1,109	1 128
TOT, PRESS RATIO	1,251	1,259	1,217	1,407	1.484
LOSS	0.0672	0,1312	0,1881	0.0424	0.0769
ADIABATIC EFFICIENCY	0.8306	0.7340	0.6423	0,9425	0.9308
TOT, PRESS LOSS PARAM	0.0148	0.0275	0.0378	0,0097	0.0173
RADIAL POSITION	~	2	6	7	2

Table 6. - Listing of Blade Element Performance (continued).

NASA TASK I (ROTOR 2D)

N.A.S.A. COMPRESSOR NUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS

					644 072	640.47	518.370) i	* * * * * * * * * * * * * * * * * * *	VELOCITY	630,121	612,258	562.583	648.605	780.400	-		VEL, KA110	106.0	404.0	0.843	1.026	1,351													
	INIET ABS	Z Z Z Z Z	0.630	0.637	50.0	20.0	0.515	204 1170		MACH NO.	0.629	0.624	0.626	0.709	0.816	CX1T DE		7 4 7 6 6 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7	/10.020.	717,121	539,358	421.672	227,022	ABS. EXTT	24	29.707	11 27B	3.8.7.82	15 072	39.059	0		086	0.9038	1758	1,98767
1967	INLET ARS	}	678,645	685.009	670.287	646.083	559,873	EXIT ABS		* PLOCIIT	726,805	716,398	722,204	805,380	917,298	TALFT PE	1110	100 TEL	C 20 TO 2 T	1000.437	979,380	860,307	724,796	ABS. TNI FT	PI ON ANG	.0			·c				# I			
:ULTS . DATE 4/27/1967	ROTOR SPD	AT INI FT	1201,225	1088.437	979,380	860.307	724,796	AGE SOTOR		A - m	1188,033	1089.059	991,397	892,423	795,383	EXIT ARS	TANG VE	150 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0.00	011.400	452,039	470,751	568,361								DRESSIBE BATTO		AUIABATIC EFF.	MONTENDERCHE	07 WEIGHT FLO	FLOW/NOZ, WEIGHT FLOW
BLADE ELEMENT PERFORMANCE RESULTS ? 19 READING NUMBFR 19 DA [*]	INLET REL	VFLACITY	1379,674	1286,053	1186,789	1076,436	915,853	EXIT REL.	> L = 00 - U >		10.1.01	747.748	779.920	777,713	754,944	INLET ABS	TANC VE				- -	•	•	TOT. TEMP	RATIO	1,148	1.136	1.152	1.142	1,151	FIXED INSTRUMENTATION B		≪ (1 2	WEIGHT FLOWIN	CHECK WEIGHT FLOW/N
DE ELEMENT PI 9 READIN	INCET REC	MACH NO.	1.2798	1,1962	1.1034	1666'0	0.8418	FXIT REL.	I CN HUN	60000	70000	0,000	0.6760	0.6846	0.6713	CH1		0.3874	0.4351	45.40	0000	0.4400	0.2530	TOT, PRESS	RATIO	1,494	1,494	1,465	1,527	1,554	FIXED INSTE	•			L.E. CHECK	T.E. CHECK
MT NUNRE	INCID ANG	SUCT.SURF	-1,939	-2.320	-2.215	-2.593	-3,452	REL, TURN	ANG! F	7.86	00.0	600.0	11,952	ټ	36.469	ST. PRESS	RISE COEFF	0.29120	0.36026	0.4004	0.400.0	0.44040	0.34235	POLYTROPIC	EFFICIENCY	0,8323	629610	0,7729	0.9128	0.9002	1.5048					06
Pol	INCID ANG	MN.CMBR.LN	1,831	2,430	3,495	3.977	3.828	REL, DEV,	ANG. T.F.	2.566	000	0 1 1 1	7.623	9.579	12,179	DIFFUSION	FACTOR	0.340	0.164	0.450	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	1800	0.327			0,8225			0,9074	0,8937	PRESSURE RATIO	351				
	REL, INLET	FLOW ANG.	60.611	57.820	55.745	23.687	54.428	REL, EXIT	FLOW ANG.	72.746	0 7 10 7	0 T C - 6 t	43.793	٠.	17.959																TRAVERSE PRE			FLOW COEFFIC	FLOW COEFFICIENT T.E	PERCENT DESIGN
	HADIAL	POSITION	-1	2	EO.	4	5	MABIAL	POSTION			,	o	4 1	ī	HADIAL	POS1710N		2	i #*7	> 🔻		u	BADIAL	POS 1 7 1 0 N		2	m	4	īU						

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

AP -		_			
TOT. TEMP RATIO	1.145	1.139	1.139	1, 133	1, 141
TOT. PRESS RATIO	1.491	1,502	1,478	1,531	1,554
LOSS COEFFICIENT	0,1126	0,0793	0,1178	0.0204	0.0542
ADIABATIC EFFICIENCY	0.8335	0,8892	0.8510	0.9771	0,9555
TOT, PRESS LOSS PARAM	0,0250	0.0172	0.0258	0,0046	0.0121
RADIAL POSITION	1	2	Э	7	5

Table 6. - Listing of Blade Element Performance (continued).

N.A.S.A. COMPRESSOR BUTPUT DATA

	INLET AX.	VELOCITY	671.448	678.759	669,071	637.848	526.728	EXTT AX.	-	626.881	693,632	542.839	626,219	652.727	AXTAL	VE PATIO	0.934	0.889	0.841	0.982	1.239									
	INLET ABS	MACH NO.	0.624	0.631	0.625	0.606	0.524	EXIT ABS	MACH NO.	0.641	0.634	0.638	0.704	0.778	EXIT REL	TANG VE	787.223	676.899	515,678	395,534	225.675	ABS.FXIT		32,598	34,330	40.209	38,434	41.117	1.5%60 0.8996 0.90%6 4.88	99548
1967	INLET ARS	VELACITY	673,524	678.842	672,305	652,710	568,900	EXIT ABS	VELOCITY	745,390	730,978	737.576	803.128	880.259	INLET REL	TANG	1201.297	1088,502	979.438	860,358	724.839	ABS, INLET	FI OW ANG.	٦.	ů.		·		лиил 100.00.	
ULTS DATE 4/27/1967	ROTOR SPE	AT INLET	1201.297	1088.502	979,438	860.358	724,839	ROTOR SPD	AT EXIT	1188.104	1089.124	991.457	892,477	795.431	FXIT ABS	TANG VE	400.881	412,225	475.779	496.942	569,756	,							10N PRESSURE RATIC ADIABATIC EFF. POLYTROPIC EFF. NOZZLE WEIGHT FLOW	FLOW/NOZ, WETGHT FLO
ELEMENT PERFORMANCE RESULTS READING NUMBER 20 DA	INLET REL	VELOCITY	1377,225	1282.845	11AB,029	1079,929	921,433	EXIT REL.	VELOCITY	1007,284	906,968	743,922	744,654	707,928	INLET ABS	TAND. VE.	0		. 0		0	TOT. TEMP	RATIO	1,165	1,151	1.162	1,151	1,153	UMENTATION B	
E ELEMENT PEI READING	INCET REC	MACH NO.	1.2763	1,1929	1.1057	1.0028	0,8490	EXIT REL.	MACH NO.	9.8559	0.7867	0.6603	0.6525	0.6259	CH1		0.4196	0.4694	0.4988	0.5050	0.3553	TOT. PRESS	RATIO	1.562	1.556	1.530	1.568	1.555	ж Ш	T.E. CHECK
BLADE POINT NUMBER 20	INCID ANG	SUCT. SURF	-1.752	-2.085	-2.298	-2.832	-3.882	AEL, TURN	AMGLE	9.329	9.779	13.166	21,170	34.922	ST. PRESS	RISE CORFF	0.32079	0.39364	0.44803	0,49375	0.44001	POLYTRUPIC	EFF101ENCY	0.8352	0.9004	0.8107	0.9139	0.9034	1.5564 1.0564 0.8697 1.980	
[Úd	INCID ANG	4N. C. 18R. LN	2.313	2.564	3.412	3.739	3.395	REL, DEV.	ANG. T.E.	1.289	3.245	6.326	8,327	13,292	DIFFUSION	FALL TOR	9.375	6.401	0.479	5.437	0.393	ADIABATIC	EFF101EUCY	0.9245	0.3940	0.464.0	0.7136	0.3973		
	MEL, INLET	Floor 446.	94.7.00	59,054	55.662	53.448	566120	TIXE THE		51,409	44.275	40.446	17.9.77	13.072															TAAVERSE POESSURE BATTO TAAVERSE ANTAHATTO EFF. TOAVERSE POLYTROPIO EFF FLOA COPFFICIENT T.E.	PERCENT DESIGN SPEED
	MADIAL	P031110%		C):	~	4	r	HADIAL	P.0.5111.0		. ~	. ~	4	ιc	MADIAL	10 11 17 CO	- - - - -	٠ ۸	· **:	4	35	H A D I A L	P0811104	- -1	~	. €	4	æ.		

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

	TOT. TEMP RATIO	1,162	1,149	1,149	1,139	1,146
-	TOT. PRESS RATIO	1,553	1,560	1.538	1,565	1,564
	LOSS	0,1300	0.0708	0.1043	0.0190	0.0845
	ADIABATIC EFFICIENCY	0.8255	0.9077	0,8763	0,9795	0,9321
	TOT. PRESS LOSS PARAM	0.0297	0.0158	0.0233	0.0044	0.0187
	RADIAL POSITION	_	2	3	4	2

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK I (ROTOR 2D)

AXIAL VFL.RATIO 1.070 1.044 1.045 1.192 1.192 EXIT AX. VFLOCITY AIL.729 AI2.473 AIG.650 AM4.799 VELOCITY VELOCITY 384.773 395.118 392.904 381.395 MACH ABS MACH NO. 0.449 0.454 0.458 0.458 GXIT REL TANG.VEL 540.615 460.647 345.755 258.349 ABS. EXIT FLOW ANG. 16,225 19,339 24,294 27,599 32,850 123,921 1,1150 0,9341 0,9357 144,32 0,97458 EXIT ABS VELOCITY 429,773 437,153 451,061 516,222 598,385 ARS, INLFT FLOW ANG, 0, 0. INLET RFL TANG, VFL 667,761 605.063 544,438 478,245 VELOCITY 385,963 395,178 394,886 390,281 342,448 4/28/1967 ADIABATIC EFF.
POLYTROPIC EFF.
NOZZLE WEIGHT FLOW/NDZ, WEIGHT FLOW
T.E. CHECK WEIGHT FLOW/NDZ, WEIGHT FLOW AT EXIT 660.428 605.408 551.118 496.099 AT INLET 667,761 605,063 544,438 478,245 EXIT ABS TANG, VEL 119,813 144,761 144,761 237,750 318,233 N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS ? 1 READING NUMBER 21 DATE EXIT REL. VELNCITY 640.158 616.339 550.340 526.027 101. TEMP RAT10 1.025 1.026 1.033 1.037 JNLFT REL VELNCITY 771,280 722.680 672.550 617.283 INLET ABS TANG, VEL 0, FIXED INSTRUMENTATION 101, PRESS 1.081 1.083 1.103 1.103 1.150 MACH NO. 0.6969 0.6536 0.6091 0.5588 EXIT REL. MACH NO. 0.6085 0.5535 0.4921 0.4717 0.1944 0.2416 0.2714 0.2493 CH1 POLYTRUPIC EFFICIENCY 0.8950 0.9910 0.8658 0.973 ST. PRESS RISE CUEFF 0,16138 0,26378 0,26940 0.27930 JNCID ANG SUCT. SURF -2.501 -3.285 -3.77 -4.852 -6.080 REL. TURN ANGLE 7.342 8.697 12.493 21.829 37.687 POINT NUMBER 1.1117 0.9415 0.9424 0.950 M. CMBR. L. 465 1. 465 1. 933 1. 718 EFFICIENCY 0.8938 0.9909 0.8639 0.9769 TRAVERSE ADIABATIC EFF.
TRAVERSE POLYTROPIC EFF.
FLOW COEFFICIENT L.E.
FLOW COEFFICIENT T.E.
PERCENT DESIGN SPEED RAVERSE PRESSURE RATIO DIFFUSION ADIARATIC REL, DEV. ANG. T.E. 3.128 5.521 6.149 8.333 FACTOR 0.175 0.241 0.266 0.253 0.161 FLUW ANG. 60.049 56.855 54.183 51.428 FLUW ANG. 52.707 48.158 41.691 29.599 14.113 RADIAL POSITION MADIAL POSITION HADIAL PUSITION CSITION 0 w 4 r 40546 4 C 10 4 L

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

TOT, TEMP RATIO	1.027	1.030	1,034	1,037	1.043
TOT. PRESS RATIO	1.084	1.098	1,108	1,135	1,159
LOSS COEFFICIENT	0,0494	0.0432	0.0567	0.0118	-0.0079
ADIABATIC EFFICIENCY	0.8518	0,8946	0.8892	0.9823	1,0078
TOT, PRESS LOSS PARAM	0,0110	9600.0	0.0128	0.0028	-0.0018
RADIAL POSITION	1	2	e	7	ç

Table 6. - Listing of Blade Element Performance (continued).

	1MLET AX. VELOCITY 367.881 377.633 373.223 360.836 298.027	EX17 AX. VELNC1TY 396.105 395.31 389.75 426.130 461.011	AXIAL VFL, RAT10 1.047 1.043 1.181 1.547	
	INLET ABS MACH NO. 0.333 0.342 0.334 0.334	EXIT ABS HACH NO. 0.377 0.383 0.383 0.46	ANG. VEL FANG. VEL FANG. VEL FASS. 758 FASS. 758 FASS. 694 FASS. 694 F	.1240 .9504 .9512 .9813 .98474
4/28/1967	10 LET ABS VELOCITY 369,019 377,691 375,078 369,243 321,889	EXIT ABS VFLOCITY 422.579 428.675 440.389 498.089	INLET RFL TANG. VEL 666.577 603.989 543.471 477.396 402.200 ARS. INLET FLOW ANG. 0.	
E	ROTOR SPD 666.577 603.989 543.471 477.396 402.200	ROTOR SPD AT EXIT 659.256 604.334 550.140 495.218	EXIT ABS TANG, VEL 144, 591 165, 577 204, 917 252, 524 320, 864	10N PRESSURE RATIO ADIABATIC EFF. POLYTROPIC EFF. NOZZLE WEIGHT FLOW FLOW/NOZ, WEIGHT FLOW
N.A.S.A. COMPRESSOR OUTPUT DATA LADE ELEMENT PERFORMANCE RESULTS 2 READING NUMBER 22 DA	INLET REL VELNCITY 761.905 742.357 660.337 663.530	EXIT REL. VELOCITY 650.035 590.639 520.702 493.178 488,994	INLET ARS TANG. VEL 0. 0. 0. 0. 107. TEMP RATIO 1.032 1.037 1.037 1.04	33
A,S,A, COMPRE DE ELEMENT PE PEADING	INLET REL MACH NO. 0.6881 0.5978 0.5978 0.5465	EXIT REL. BACH NO. 0.5802 0.5276 0.4648 0.4415	CH1 0.2479 0.2923 0.3184 0.2989 0.0538 TOT, PRESS RATIO 1,110 1,116 1,116 1,116	FIXED INSTRUMENTATION L.E. CHECK WEIGHT FLO T.E. CHECK WEIGHT FLO
B NT NUMBER	INCID ANG SUCT. SURF -1.444 -2.155 -2.439 -3.364 -4.418	REL, TURN ANGLE 8,689 10,009 13,953 23,254 38,813	ST. PRESS RISE COEFF 0.21139 0.27267 0.31604 0.33015 0.1780PIC EFFICIENCY 0.9623 0.9362 0.9362	1.1240 0.9358 0.9369 0.960 0.950
104	INCID ANG MN.CMBR.LN 2.326 2.595 3.271 3.206	REL, DEV, ANG, T.E. 2.237 2.946 5.398 6.213 8.869	DIFFUSION FACTOR 0.216 0.229 0.208 0.203 ADIARATIC FFICIENCY 0.9280 0.9417 0.9349	0 • 4.
	REL, INLET FLOW ANG. 61,106 57,985 55,521 52,916 53,462	FLOW ANG. 52.417 47.976 41.568 29.663 14.649		TRAVERSE PRESSURE RAT TRAVERSE ADJAHATIC EF TRAVERSE POLYTROPIC E FLOW CREFFICIENT L.E. FLOW CREFFICIENT T.E.
	#AB1AL P0S11AL 1 1 2 3 3 5 5	MADIAL POSITION 2 3 3 5	HADIAL POSITION 1 1 2 3 4 5 5 6 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	

	TOT. TEMP RATIO	1,032	1,033	1,036	1,038	1 042
TRUMENTALION	TOT, PRESS RATIO	1,101	1,112	1.118	1,140	1.158
FROM FIXED INS	LOSS COEFFICIENT	0.0541	0.0307	0.0474	-0.0004	-0.0175
PAKAMETEKS DETERMINED FROM FIXED INSTRUMENTATION	ADIABATIC EFFICIENCY	0.8646	0,9328	0,9151	1,0005	1.0167
PAKAI	TOT. PRESS LOSS PARAM	0.0121	0,0069	0.0108	-0,0000	-0.0040
	RADIAL POSITION	1	2	٣	7	2

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK ! (ROTOR 2D)

VELOCAX. VELOCAX. UNYO.500 UNSO.418 UNSO.917 UNYO.500 AXTAL VFL.RATIO 1NLET AX. VELOCITY 389.675 349.156 346.039 332.678 1.091 1.055 1.031 1.176 MACH ABS 0.307 0.315 0.315 0.314 0.307 320,201 225,401 109,958 FLOW ANG. 26.443 28.551 32.870 34.655 38.833 0.373 0.373 0.426 0.486 TANG VEL 475.825 FXIT ARS 404.639 IBS.EXIT FXIT REL HACH 1.1400 0.9445 0.9456 127.22 0.98487 VELDCITY 340,725 349,209 347,758 346,479 INLET RFL 667,418 664,752 544,158 477,999 ABS, INLET FLOW ANG. 419,435 478.015 538.453 414.602 EXIT ABS VELOCITY 4/28/1967 ADIABATIC EFF.
POLYTROPIC EFF.
NOZZLF WEIGHT FLOW
T.E. CHECK WEIGHT FLOW/NOZ, WEIGHT FLOW
T.E. CHECK WEIGHT FLOW/NOZ, WEIGHT FLOW PRESSURE RATIO AT EXIT 660.089 605.097 550.835 441.927 ROTOR SPD AT INLET 667.418 604.752 544.158 477.999 EXIT ABS TANG. VEL 184.264 200.459 230.634 270.443 DATE N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS R 3 READING NUMBER 23 DAI TOT, TEMP RAT10 1,039 VELNC TY VELNC TY 749,360 698,335 645,789 586,835 502,197 INLFT ABS TANG, VEL 0. 0. 0. 603,615 547,243 479,863 454,054 437,972 EXIT REL. VELNCITY FIXED INSTRUMENTATION 1.040 1.043 1,039 MACH NO. 0.6748 0.6301 0.5628 0.5295 0.4522 TOT. PRESS MACH NO. 0.5354 0.4864 0.4264 0.4047 0.3077 0.3545 0.3833 0.3728 0.1814 EXIT REL RATIO 1.127 1.133 1.133 CHI ST. PRESS RISE COEFF 0.26821 0.33359 0.38118 0.40665 EFFICIENCY 0.8896 0.9446 0.9021 0.9669 INCID ANG SUCT. SURF 0.477 -0.1140 -1.117 -2.480 POLYTROP IC REL, TURN POINT NUMBER ANGLE 10.933 12.317 15.651 25.214 0.9333 0.9346 0.980 0.950 1.1406 MN. CMBR. LN EFFICIENCY 0.8876 0.9436 0.9003 0.9662 0.9717 TRAVERSE ADIABATIC EFF.
TRAVERSE POLYTROPIC EFF.
FLOW COEFFICIENT L.E.
FLOW COEFFICIENT T.E.
PERCENT DESIGN SPEED ANG. T.E. 1.914 2.653 5.726 6.498 9.149 FACTOR 0.284 0.312 0.356 0.358 0.353 ADIABATIC RAVERSE PRESSURE RATIO 4.610 5.297 5.453 4.800 FLOW ANG. 63,027 60,000 57.547 55.163 REL, FXIT FLOW ANG. 52.094 47.683 41.896 20.948 14.929 MADIAL PUSITION RADIAL POSITION HADIAL PGSITION NOITION HABIAL 0 m 4 m 11 CM 4 CM

TOT. TEMP RATIO	1,039	1,039	1,040	1,041	1.044
TOT. PRESS RATIO	1.126	1.132	1,135	1.150	1,162
LOSS COEFFICIENT	0.0597	0.0381	0.0489	0.0080	0,0102
ADIABATIC EFFICIENCY	0,8798	0.9314	0.9251	0.9900	0,9912
TOT. PRESS LOSS PARAM	0.0135	0.0086	0.0110	0.0019	0.0023
RADIAL POSITION	-	2	3	寸	5

- Listing of Blade Element Performance (continued), Table 6.

VFL.RATIO 1.086 1.039 1.027 1.147 1.495 VELOCITY 3384.194 348.902 348.902 338.163 361.905 VELOCITY 326.227 325.647 339.647 329.341 315.424 389,321 310,591 217,114 108,377 ABS. EXIT PLOW ANG. 29.545 31.716 35.376 37.590 40.490 EXIT ABS D 361 0 361 0 364 0 468 0 468 0 468 EXIT REL TANG.VEL 459.157 0.9221 0.9236 122.02 0.98498 0.96234 1 N L ET A B S VELOCITY 327.236 335.698 330.977 322.773 INLET RFL TANG, VFL 667,249 407,889 410,164 415,112 458,879 521,889 604.599 544.020 477.878 402.605 ABS. INLFT FLOW ANG. EXIT ABS VELOCITY 4/28/1967 ADIABATIC EFF.
POLYTROPIC EFF.
NOZZLE WEIGHT FLOW
CHECK WEIGHT FLOW/NOZ, WEIGHT FLOW
CHECK WEIGHT FLOW FIXED INSTRUMENTATION PRESSURE RATIO AT EXIT 659.922 604.944 550.696 495.718 ROTOR SPD AT INLET 667.249 604.599 544.020 477.878 EXIT ABS TANG.VEL 200.764 215.623 240.104 278.604 333.438 N.A.S.A. COMPRESSOR GUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS R 4 READING NUMBER 24 DATA 1NLFT REL VELNCITY 743.172 601.544 636.792 576.672 107, TEMP 1.044 1.042 1.043 1.043 1.044 INLET ABS TANG. VEL 0. 0. 0. 580,425 522,793 459,494 424,368 415,851 EXIT REL. VFLOCITY 101. PRESS 1.140 1.143 1.143 1.153 1.153 MACH NO. 0.6695 0.6238 0.5247 0.5205 EXIT REL. MACH NO. 0.5142 0.4639 0.4079 0.3780 0.3455 0.3938 0.4208 0.2344 CHI POLYTROPIC EFFICIENCY 0.8841 0.9426 0.8912 0.9556 ST. PRESS RISE COEFF 0.30450 REL. TURN ANGLE 11.592 12.829 16.244 25.613 SUCT. SURF 1.395 0.823 0.850 0.293 INCID ANG 0.37239 0.41917 0.44543 0.36019 POINT NUMBER 1.1483 0.9260 0.9275 0.980 MN.CMBR.LN 5.165 5.573 6.560 6.863 6.114 ADIAGATIC FFFICIENCY TRAVERSE ADIABATIC EFF.
TRAVERSE POLYTROPIC EFF.
FLOW COEFFICTENT 1.E.
FLOW COEFFICTENT 1.E.
PERCENT DESIGN SPEED D1FFUSION FACTOR 0.318 0.348 0.393 0.397 REL. DEV. 2.173 2.174 3.104 6.396 7.510 NCID ANG TRAVERSE PRESSURE RATIO 0.9415 0.8891 0.9547 0.9710 0.8819 REL, INLET FLUW ANG, 63.945 FLOW ANG. 52.353 48.134 42.566 30.960 15.509 60.963 58.810 56.573 57.014 MADIAL POSITION RADIAL POSITION POSITION MOILISC BABIAL RADIAL

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

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	TOT, TEMP RATIO	1,045	1,043	1,043	1,044	1,046
NOT TUT WILION TO	TOT. PRESS RATIO	1,139	1,144	1,144	1,156	1,166
The same of the same of	LOSS COEFFICIENT	0.0875	0.0563	0.0700	0.0253	0,0173
NOTIVINIONIONI GRAFI HONE GRAFIES CONTRACTOR	ADIABATIC EFFICIENCY	0.8464	0,9098	0,9035	0.9710	0,9859
	TOT. PRESS LOSS PARAM.	0.0196	0.0126	0.0156	0.0059	0.0039
	RADIAL POSITION	1	2	٣	7	2

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK I (ROTOR 2D)

	INLFT AX. VELOCITY 385.867 345.891 342.377 360.549	EXIT AX. VELOCITY 336,951 327,632 346,3314 369,860	AXIAL AXIAL 1.02 1.037 1.015 1.142 1.484	
	INLET ABS MACH NO. 0.275 0.283 0.283 0.277	EXIT ABS HACH NO. 0.356 0.356 0.356 0.356 0.356	TANG VEL 4ANG VEL 341,928 290,872 211,580 104,427 104,427 104,427 104,427 103,089 35,461 39,378 42,393	.157n .9253 .9268 .61 .99527
4/28/1967	JNLET ARS VELOCITY 306.812 315.939 343.930 307.552	XII ABS ELOCITY 402.77 410.35 447.81 508.48	INLET ABEL ABNG. CFL 504.9631 478.1344 478.1341 ADS. INLFT FLOW NG. 0.0.0.00000000000000000000000000000	11 11 11 H H
A TS DATE	ROTOR SPD AT INLET 667.631 604.945 544.331 478.151	ROTOR SPD AT EXIT 660.299 605.290 551.010 442.067	EXIT ABS TANG VEL 219,398 233,362 284,422 337,641	TION PRESSURE RATIC ADIAHATIC EFF. POLYTROPIC EFF. NOZZLE WEIGHT FLOW FLOW/NOZ. WEIGHT FLOW
COMPRESSOR OUTPUT DATA ENT PERFORMANCE RESULTS EADING NUMBER 25 DAT	INLFT REL VFLNCITY 734.755 682.477 626.369 548.522 484.485	A + 4 + 6 0 4 + 4 + 4 + 4 + 4 + 4 + 4 + 4 + 4 + 4	TANGT ABS TANGT VEL 00.00.00.00.00.00.00.00.00.00.00.00.00.	UMENTATION P A A WEIGHT FLOWIN WEIGHT FLOWIN
S.A. C ELEME RE	INLET REL MACH NO. 0.6611 0.5663 0.5663 0.5122	EXIT REL. MACH NO. 0.4905 0.3812 0.3601	0.3745 0.4223 0.4515 0.4504 0.2970 1.152 1.153 1.153 1.150	FIXED INSTRUMENTATION L.F. CHECK WEIGHT FLO T.E. CHECK WEIGHT FLO
B NT NUMBER	INCID ANG SUCT. SURF 2.836 2.287 2.190 1.568	REL. TURN ANGLE 12.774 13.804 17.605 26.203 42.491	NISE COEFF 0.35260 0.45066 0.48820 0.42680 0.42680 0.9269 0.9327 0.9405 0.9405	1.1564 0.9090 0.9109 0.9109 0.950
104	INCIP ANG AN.CMBR.LN 6.606 7.037 7.900 8.138	ANG. 1.E. 2.432 3.593 6.375 9.987	ADIABATIC PEFFICE P	
	REL, INLET FLOW ANG, 65,386 62,427 60,150 57,848	PEL. EXIT FLUW ANG. 52.512 48.623 42.545 31.645 15.767		THAVERSE PRESSURE RATIO TRAVERSE ADIABATIC EFF. TRAVENSE POLYTROPIC EFF FLOW COEFFICIENT L.E. FLOW COEFFICIENT T.E.
	HADIAL DOSITION 2 1 100N 3 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		0	

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

T. PRESS A SS PARAM E	ADIABATIC SFFICIENCY	LOSS COEFFICIENT	TOT. PRESS RATIO	TOT, TEMP RATIO
	0.8320	0,1065	1,150	1.049
	0.9262	0.0493	1.154	1.045
	0,9148	0,0655	1,151	1.045
	0.9830	0.0155	1,161	1.044
	0,9873	0,0165	1,171	1,047

Table 6. - Listing of Blade Element Performance (continued).

N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS

	INLET AX.	VELOCITY	286.A30	907 943		293.11/	278.424	233,141	EXIT AX.	VELOCITY	314.014	309.186	292,948	322.859	346.921	AXIAL	VEL . RATIO	1.095	1.040	0.999	1.160	1.488									
	INLET ABS	CZ	0.00			0.265	0.257	0.227	FXIT ABS	¥							TANG.VEL	409.726	352,122	267.074	194,512	94,534	ABS.EXIT	FLOW ANG.	38.470	39,203	44.015	42,964	44.992	1,1640 0,9138 0,9157 19,52	1,98070 1,95827
1967	INLET ARS	VELDITA	287 747	440.000	000110	294,574	284.911	251,808	EXIT ABS	VELOCITY	401,673	399,004	407,640	442.971	497,463	INLET REL	TANG. VEL	666.554	603,969	543,453	477,380	402,186	ABS. INLET	FLOW ANG.	ó	.0	٥.	c	•	n u u r	
DATE 4/28/1967	ROTOR SPD	AT THE ET	- 1 1 1 1 1 W	670	903.969	543.453	477.380	402,186	ROTOR SPD	AT EXIT	659.234	604,313	550,121	495,201	441,354	EXIT ABS	TANG.VEL	249,508	252,191	283.047	300,689	346.820						,		PRESSURE RATIO ADIABATIC EFF. POLYTROPIC EFF NOZZLE WEIGHT	FLOW/NOZ, WEIGHT FLOW FLOW/NOZ, WEIGHT FLOW
READING NUMBER 26	INLET REL		700 000	170.179	0/2:1/0	648.154	555,937	474,511	EXIT REL.	VELOCITY	516.684	468,608	396,715	379,005	368,947	INLET ABS	TANG. VE					0	TOT. TEMP	RATIO	1.057	1.049	1,050	1.048	1,049	INSTRUMENTATION F	WEIGHT FLOW/NOZ. WEIGHT FLOW/NOZ.
READING	TALET REL			/200.0	10000	0.5569	0.5008	0,4271	EXIT REL.	A	0.4544	0.4141	0.3508	0.3365	0.3290	CH 143		0.3968	0.4441	0.4715	0.4682	0.3361	TOT. PRESS	4110	1,163	1,161	1.157	1.164	1.174	FIXED INSTA	L.E. CHECK
POINT NUMBER A	TNC 10 ANG		*********	/ot - 1	3.626	3.699	3.468	2.020	REL. TURN	ANGLE	181.181	15.081	19.305	28.680	44,657	ST. PRESS	RISE COFFF	35448	40304	0.47+84	0.50901	0.47167	POLYTROPIC	FFFICIENCY	0.7774	0.8870	0.8485	0,9296	0.9644	1,1635 0,8689 0,8717	= 0.950 = 50
104	SNA CIONT		AN.CABK.LN	/56·/	8.406	9.409	10.038	9.300	RFL. DEV.		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	3.685	6.1.05	7.618	9.463	PIFFUSION	FACTOR	4.4	4 4 4	40.0	7.4	0.401	ADIABATIC	A DE LO LEGICA	0.7726	0.8845	0,8453	0.9281	0.9636		TENT T.E.
	F 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		FLOW ANG.	66.71/	63.796	61,659	5.0	006.66	PEI PYIT			1000 A	40 447	840.45	15.243															TRAVERSE PRE TRAVERSE ADI TRAVERSE POL	FLOW COEFFICIENT T.E. PERCENT DESIGN SPEED
		141046	PUSITION	-1	2	m	4	rus	I A D T A I			۰ ۵	u m	o •	חוי	14 10 4 5		201-10-1	4 C	u P	γ 4	r un	14 20			۰,۰	J PC	4	· W		

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

TOT, TEMP RATIO	1.055 1.048 1.047 1.046 1.046
TOT. PRESS RATIO	1, 160 1, 163 1, 158 1, 166 1, 175
LOSS	0, 1477 0, 0573 0, 0738 0, 0192 0, 0043
ADIABATIC EFFICIENCY	0, 7929 0, 9207 0, 9105 0, 9804 0, 9969
TOT. PRESS LOSS PARAM	0.0330 0.0127 0.0165 0.0044 0.0010
RADIAL POSITION	5 4 3 3 2 2 1

Table 6. - Listing of Blade Element Performance (continued).

N.A.S.A. COMPRESSOR AUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS ' POINT NUMBER 7 READING NUMBER 27 DATE 4/28/1967

	INLFT AX. VELOCITY 946.030 552.865 547.462 531.057 440.310	EXIT AX. VELOCITY 574.359 556.481 522.031 618.276	AX1AL VFL. RATTO 1.052 0.954 1.164 1.524	
	INLET ABS MACH NO. 0.502 0.507 0.505 0.499	EXIT ABS MACH NO. 0.527 0.529 0.529 0.529	EXIT REL 78NG VEL 758.206 654.529 485.505 365.830 186.258 186.258 16.058 19.042 28.647 27.940	.2150 .9006 .9034 .52 .99307
1967	INLET ARS VELOCITY 547,748 552,949 550,182 543,431	VELOCITY 599.028 588.714 595.473 703.954.	INLET REL 4005. VEL 846.112 761.334 668.772 568.772 568.772 700. NCFT FLOW ANG.	# H H H H H H
DATE 4/28/1967	ROTOR SPD AT INLET 933.789 846.112 761.334 668.772 563.430	ROTOR SPD AT EXIT 923.534 846.595 770.677 693.738 618.302	EXIT ABS TANG VEL 165.328 192.086 285.172 327.908 432.045	TION PRESSURE RATIO ADIABATIC EFF. POLYTROPIC EFF. NOZZLE WEIGHT FLOW FLOW/NOZ. WEIGHT FLOW
NUMBER 27	INLET REL VELOCITY 1082,570 1010,771 939,324 861,726	EXIT REL. VELNCITY 952.039 859.129 743.428 774.602	INLET ABS TANG. VEL 0. 0. 0. 0. 1.077 1.052 1.052 1.052 1.052 1.052 1.052	CUMENTATION P A A HFIGHT FLOWIN WEIGHT FLOWIN
READING NUMBER	INLET REL MACH NO, 0,9913 0,9267 0,8620 0,7907	EXIT REL. MACH NO. 0.8550 0.7696 0.6341 0.6484	CH1 0.1896 0.2403 0.2563 0.2640 0.0184 107, PRESS PATIO 1.153 1.169 1.169 1.261 1.316	FIXED INSTRUMENTATION L.E. CHECK WEIGHT FLO T.E. CHECK WEIGHT FLO
NT NUMBER 7	INCID ANG SUCT.SURF -2.867 -3.301 -3.679 -4.732	REL, TURN ANGLE 6.828 7.210 11.357 20.935 36.482	ST. PRESS RISE COEFF 0.14241 0.20977 0.23886 0.12505 0.12505 POLYTROPIC EFFICIENCY 0.8861 0.9148 0.9148	1.2090 0.8579 0.8617 0.980 0.950
HO4	1NC1D ANG MN.CMBR.LN 0.903 1.449 2.031 1.393	REL, DEV. ANG, T.E. 2.675 4.599 6.754 7.103	DIFFUSION FACTOR 0.176 0.333 0.266 0.174 ADIABATIC FFICIENCY 0.8810 0.6376 0.9120	PRESSURE RATIO = ANIAHATIC EFF, = POLYTROPIC EFF, = FICIENT L.E. = FICIENT 1.E. =
	REL INLET Flow ANG. 59.683 56.839 54.281 51.548 51.993	REL, EXIT FLOW ANG, 52,855 49.629 42.924 30.613		TRAVERSE PRESSURE RATIO TRAVERSE ANIAHATIC EFF TRAVERSE POLYTROPIC EFF FLOW COEFFICIENT L.E. FLOW COEFFICIENT 1.E.
	HADIAL PUSITION 1 2 3 3 5 5	#ADJAL DOSITION 2 3 3 5	MADIAL 21110N 2233 344 551710N 572140N 533740N	

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

TOT, TEMP RATIO	1,050	1,055	1.065	1.071	1.081
TOT. PRESS RATIO	1,159	1,176	1,185	1,261	1,313
LOSS COEFFICIENT	0.0489	0.0564	0.1324	0.0216	0.0027
ADIABATIC EFFICIENCY	0.8504	0.8667	0.7602	0,9689	0,9974
TOT. PRESS LOSS PARAM	0.0108	0.0122	0.0294	0.0050	0,0006
RADIAL POSITION	-	2	3	t,	?

Table 6. - Listing of Blade Element Performance (continued).

VFL.RAT10 0.994 EXIT AX. VFLOCITY 520.911 505.692 505.583 533.397 564.087 VELOCITY 523.988 526.096 515.710 489.018 INLET ABS MACH NO. 0.480 0.481 0.474 0.457 FLOW ANG. 26.822 29.327 33.187 35.804 39.186 EX1T REL TANG.VEL 660.002 562,360 439,872 308,874 158,373 EXIT ABS MACH NO. 0.516 0.513 0.534 0.588 1.2910 0.9471 0.9490 179.75 0.98677 0.96645 INLET RFL 933.636 935.973 845.973 761.210 668.662 JNLFT ABS VELNCITY 525.609 526.176 518.272 500.412 584.845 580.047 604.701 660.935 740.064 ABS.INLET FLOW ANG. EX1T ABS FIXEN INSTRUMENTATION PRESSURE RATIO ADIABATIC EFF.
POLYTROPIC EFF.
NOZZLE WEIGHT FLOW.
T.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW 4/27/1967 AT EXIT 923.383 846.457 770.550 693.624 618.201 ROTOR SPD 41 INLET 933.636 845.973 761.210 668.662 563.338 EXIT ABS TANG.VEL 263.380 284.096 330.678 364.751 ELADE ELEMENT PERFORMANCE RESULTS
R B READING NUMBER 28 DATE EXIT REL. VELOCITY 841.592 756.302 670.674 619.843 INLET RFL VFLOCITY 1071.420 996.259 920.894 835.177 TOT. TEMP RATIO 1.079 1.074 1.086 1.085 INLET ABS TANG, VEL O. TOT, PRESS RATIO 1.271 1.278 1.313 1.313 EXIT REL-MACH NO. 0.7423 0.6592 0.5927 0.5511 INLET REL MACH NO. 0.9783 0.9106 0.8430 0.7634 0.3491 0.3968 0.4249 0.4090 CH3 ST, PRESS PISE COEFF 0.28501 0.35232 0.40115 0.42373 EFFICITYON 0.8998 0.9812 0.9812 0.9585 0.9584 RFL. TURN ANGLE 8.990 10.086 14.850 23.747 SCCT. SURF -1.853 -2.017 -2.077 -2.459 -3.546 1.2945 6.9364 6.9331 6.980 0.980 POINT NUMBER THAVERSE PUESSURE RATIO TEAJERSE ANIMARTIC EFF. THAVERSE POLYTROPIC EFF. FLOW CCEPFICIENT 1.E. CLOW CEFFICIENT 3.E. PERCENT DESIGN SPEED. 1.917 2.733 3.633 3.734 3.734 3.734 401484710 EFF.01E40Y 0.963 0.9405 0.9570 0.9570 PIFFUSION FACTOR 0.304 0.336 0.336 0.344 AEL DEV. ANG. T.F. 1.536 3.007 4.354 6.624 9.963 7.7. 7.0. 2007 1008 5008 RADIAL POSITION RADIAL POSITION RADIAL POSITION 1 2 3 4 4

40° 10° 40°

47 W 4 W

0.961 0.980 1.091 1.395

AXIAL

TOT. TEMP RATIO	1, 078 1, 077 1, 080 · 1, 081 1, 086
TOT. PRESS RATIO	1,268 1,279 1,283 1,306 1,329
LOSS	0.0545 0.0343 0.0515 0.0130 0.0212
ADIABATIC EFFICIENCY	0, 8996 0, 9429 0, 9260 0, 9843 0, 9818
TOT. PRESS LOSS PARAM	0.0124 0.0077 0.0118 0.0030 0.0048
RADIAL POSITION	1 2 2 3 3 4 4 4 5 5 5

Table 6. - Listing of Blade Element Performance (continued).

	INLET AX. VFLNC.1TY 563.002 587.792 498.678 478.297	EXIT AX. VELNCTTY 498.018 487.403 474.984 490.998 529.788	AXIAL VEL.RATIO 0.990 0.960 0.952 1.045	
	INLET ABS MACH NO. 0.460 0.464 0.458 0.447	EXIT ABS HACH NO. 0.505 0.507 0.507 0.507 0.519	FX17 RFL 17ANG.VFL 637,310 541,480 423,361 300,174 151,297	ABS. EXTT FLOW ANG. 29,859 36,152 36,154 41,383
4/28/1967	10 LET ARS VELOCITY 504.557 507.869 501.156 489.441	EXIT ABS VFLOCITY 575.304 574.886 588.787 639.115	IALET RFL TANG, VFL 933,462 845,816 761,068 668,538 563,233	ABS. INLET PLOW AND OF CO.
S ATE	ROTOR SPD AT INLET 933.462 845.816 761.068 668.538	AT EXIT 923,211 846,299 770,407 693,495	EXIT AHS TANG, VEL 2A5,901 304,818 347,046 393,321 466,789	
", A' COMPRESSOR OUTPUT DATA ELEMENT PERFORMANCE RESULTS READING NUMBER 29 DA	INLFT REL VELNCITY 1061,098 986,578 911,253 828,550	EXIT REL. VFLNCITY 8n9.567 728.547 536.761 586.405	INLET ABS TANG. VEL 0. 0. 0.	TOT. TEMP RATIO 1.084 1.088 1.088 1.088
N.A.S.A. COMPRESSOR OUTPUT DATA LADE ELEMENT PERFORMANCE RES ^U LT 9 READING NUMBER 29 D	INLET KEL MACH NO. 0.9664 0.9013 0.8324 0.7564	EXIT REL. MACH NO. 0.7112 0.6420 0.5611 0.5193	CH1 0.3839 0.4324 0.4657 0.4671	101, PRESS RATIO 1,299 1,305 1,325 1,344
B NT NUMBER	INCID ANG SUCT.SURF -0.868 -1.119 -1.194 -1.861	REL, TURN ANGLE- 9.687 11.013 15.055 23,440 39,145	ST. PRESS RISE COEFF 0.31819 0.38754 0.44263 0.48289	POLYTROPIC EFFICIENCY 0.9258 0.9452 0.9102 0.9405
10 d	INCID ANG MN.CMBR.LN 2.902 3.631 4.516 4.709	9EL, DEV, ANG, T.E. 1.815 2.979 5.541 7.529 10.158	DIFFUSION FACTOR 0.335 0.355 0.417 0.422	ADIARATIC FFICIENCY 0,9229 0,9431 0,9967 0,9950
	RFL, INLET FLUN ANG. 61.682 59.021 56.766 54.419	FLUW ANG. 51.995 48.009 41.711 30.979 15.938		
	MADIAL POSITION 1 2 2 3 4 5	MADIAL POSITION 1 2 3 4 5	MADIAL POSITION 1 2 3 4 5	MADIAL PGSITION 1 2 3 4 5

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

1.3130 0.9683 0.9695 174.55 0.99037

FIXED INSTRUMENTATION PRESSURE RATIO **
ADIABATIC EFF. **
POLYTROPIC EFF. **
NOZZLE WEIGHT FLOW/NOZ. WEIGHT FLOW **
T.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW **

1.3139 0.9342 0.9367 0.980 0.950

THAVERSE ADIAHATIC EFF. # 0
THAVERSE ADIAHATIC EFF. # 0
THAVERSE POLYTROPIC EFF. # 0
FLOW COEFFICTENT L.E. # 0
FLOW COEFFICTENT T.E. # 0
PERCENT DESIGN SPEED

SFFICIENCY COEFFICIENT

Table 6. - Listing of Blade Element Performance (continued).

MACH NO. 0.457 0.451 0.451 0.451 0.432 MACH ABS 0.502. 0.506 0.506 0.506 FX1T RFL TANG. VFL 630.881 529.793 416.139 294.181 151.526 FLOW ANG. 80.848 83.479 87.138 86.813 EXIT ABS VELOCITY 572.807 575.141 588,440 640.984 TANG. VFL. 934.289 846.565 761.742 669.129 563.732 501,869 504,888 494,339 474,311 413,644 DATE 4/28/1967 RDTOR SPD AT INLET 934.289 846.565 761.742 669.129 563.732 AT EXIT 924,028 847,048 771,089 694,109 EXIT ARS TANG.VEL 293.147 317.256 354.950 399.928 N.A.S.A. COMPRESSOR NUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS ? 10 HEADING NUMBER 30 DATA INLFT REL VELOCITY 1060.551 985.680 908.087 820.186 EXIT REL. VELNCITY 800.114 744.214 627.251 580.914 540.422 101. TEMP RATIO 1.088 1.090 1.090 1.093 107. PRESS 1307 1313 1313 1327 1327 INLET REL MACH NO. 0.9659 0.8997 0.4287 0.7478 EXIT REL MACH NO. 0.7016 0.6290 0.5518 0.5140 0.3949 0.4433 0.4721 0.4568 CHI POLYTROPIC EFFICIENCY 0,9084 0,9563 0,8988 0,9426 0,9560 ST, PRESS 0.32854 0.39830 0.44942 0.47438 INCID ANG SUCT. SURF -0,720 -0,948 -0,812 -0,991 -2,071 REL, TURN ANGLE 9.716 11.352 15.546 24.677 39.786 POINT NUMBER INCID ANG MN, CMBR, LN 3,050 3,802 4,898 5,579 5,579 ADIABATIC FFICIENCY 0.9048 0.9545 0.8949 0.9402 FACTOR 0,346 0.383 0.428 0.425 0.362 REL. DEV. ANG. T.E. 1.932 2.810 5.431 7.163 FLUW ANG. 61.830 59.192 57.148 55.289 FLOW ANG. 52.112 47.440 41.601 30.613 84014L POSITION 1 2 3 3 MADIAL POSITION 1 2 3 4 5

₩ 0/ 10/ 4 C

VELOCITY 490.912 499.707 479.707 468.689 497.184

560.322 504.811 491.895 463.512 382.981

AX1AL VFL.RAT10 0.981 0.950 1.073 1.370

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

TOT. TEMP RATIO	1.089 1.086 1.086 1.085
TOT. PRESS RATIO	1, 307 1, 317 1, 312 1, 324 1, 341
LOSS	0.0662 0.0347 0.0467 0.0125 0.0168
ADIABATIC EFFICIENCY	0,8934 0,9487 0,9389 0,9860 0,9865
TOT. PRESS LOSS PARAM	0.0149 0.0078 0.0106 0.0029 0.0038
RADIAL OSITION	Z E 4 S

RADIAL 20SITION 1 2 3 5

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK ! (ROTAR 2D)

N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS

	INLET AX.	VELOCITY	464.304	471.247	461.532	437,837	561,232	EXIT AX.	VELOCITY	460.447	449.470	421.828	449.025	460.394	AXIAL	VEL . RATIO	0.992	0.954	0.914	1.026	1.330									
	INLET ABS	MACH NO.	0.423	0.429	0.422	0.408	0.353			0.500					EXIT REL	TANG, VEL	583,868	497,135	390,113	278.270	138,932	ABS. FX1T	FLOW ANG.	36.476	37,919	42,103	45.816	44.969	1,3460 0,9407 0,9431	. 461 . 98868 . 95533
1967	INLET ARS	VELOCITY	465,739	471,319	463,826	448,038	390,194	EXIT ABS	VELOCITY	573,524	569,772	568,974	614,609	688,587	INLET REL	TANG, VEL	934,545	846,797	761,951	669,313	563,887	ABS. INLET	F) OF ANG				•	•		M9T # # 30
DATE 4/28/1967	ROTOR SPD	AT INLET	934,545	846.797	761,951	669,313	563,887	ROTOR SPD	AT FX1T	924,282	847,281	771,300	694.299	618,803	EXIT ABS	TANG. VEL	340.414	350,146	381,187	416.029	479.871								PRESSURE RATIO ADIABATIC EFF. POLYTROPIC EFF.	NOZZLE WEIGWT FL FLOW/NOZ, WEIGHT FLOW FLOW/NOZ, WEIGHT FLOW
ELEMENI PERFURMANCE RESULIS READING NUMBER 31 DA	INLPT REL	VELACITY	1044,168	969.127	892,022	805,430	685.703	EXIT REL.	VELOCITY	744.278	670,210	574,992	531,128	513,010	INLFT ABS	TANG. VE	0													WEIGHT FLOW/ Weight Plow/
E ELEMENI PERFURMAN KEADING NUMBFR	INLET REL	MACH NO.	0.9483	0.8826	0.8122	0.7332	0,6212	EXIT RELA	I C	0.6483	0.5868	0.5036	0.4682	0.4548	CH1	ı	0.4388	0.4873	0.5150	0.5173	0,3999	TOT PRESS	0 1 1 0	1,354	1.350	1.330	1,541	1,360	FIXED INSTRUMENTATION	T.E. CHECK
BLADE INT NUMBER 11	INCID ANG	SUCT. SURF	1.031	0.764	0.836	0.529	-0.524	NEU TURN		11.041	13.021	16.033	25.022	41,226	ST. PRESS	BISE CORFE	0.37452	0.44303	0.404.0		0.51493		>L2U+1-11U	0.8911	0,9383	0,8920	0,9422	0,9674	m 1.3474 m 0.9191 m 0.9225	
04	INCID ANG	MN, CMBR, LN	4.801	5.514	2.4	7.009	6.756	DEV.		1.560	2.853	6.593	8 337	10.350	NIFFIISTON	10.00 LV V		000	2 2 2 2	0.482	0.423		> C 2 0 + C - C - C - C - C - C - C - C - C - C	0.8863	0.9356	5	0.9398	0,9659	PRESSURE RATIO ADIMBATIC EFF. POLYTROPIC EFF.	TENT L.E. TENT T.E. SPEED
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	NA MOLE	64.584	400.00	700	0000	57.356	- NO 100	1	2 A A A C	7 T T T T T T T T T T T T T T T T T T T	42.763	44 7 23	16.130															TRAVERSE PRE TRAVERSE ADI TRAVERSE POL	
	Q Q Q	NO P P CO		10	J F	> ◀	r un	4			۰ ،	J P	•	run	- 4			٦.	~ P	າ ◀	יט ז		SAULAL SOCIETION	201 - 1001	٠, ٥	נייו נ		. rv		

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

TOT. TEMP RATIO	1, 103 1, 095 1, 092 1, 089	1.091
TOT. PRESS RATIO	1,350 1,351 1,333 1,343	1,355
LOSS COEFFICIENT	0.0971 0.0382 0.0576 0.0146	0.0091
ADIABATIC EFFICIENCY	0.8664 0.9495 0.9311 0.9850	0,9931
TOT. PRESS LOSS PARAM	0.0221 0.0086 0.0128 0.0034	0,0020
RADIAL POSITION	7 3 5 1	5

Table 6. - Listing of Blade Element Performance (continued).

, W.A.S.A. COMPRESSOR GUTPUT DATA

	INCET AX.	485.713	443,682	429,364	408.574	335,670	EXIT AX.	VFLOCITY	429,245	415.680	377,317	431.840	461,572	AXIAL	VFL. RATIO	0.985	0.937	0.879	1.057	1.375									
	INLET ABS	3.396	0.404	0.393	0.380	0.328	EXIT ABS	MACH NO.	0.496	0.492	0.494	0.541	909.0	EXIT REL	TANG. VEL	546.114	465.730	349.280	259.037	125.648	ABS, EXIT	FLOW ANG.	41.248	42,428	48.102	45.139	46.827	0.4 %	.99349 .95300
4/27/1967	INLET ABS	437,060	443.749	431.497	418.093	362,545	EXIT ABS	VELOCITY	571.700	563.170	565.357	614.498	683.510	INLFT REL	TANG, VEL	932.773	845.192	760.506	668.044	562.818	ARS.INLET	FLOW ANG.		٥.	٥.	0.	.0		6.0 H H
TE 4/27	ROTOR SPD				668.044	562.818	ROTOR SPD	AT EXIT	922.530	845.674	769.838	692.983	617.630	EXIT ARS	TANG, VEL	376.416	379.944	420.559	433,947	491.982								TION PRESSURE RATIO ADIABATIC EFF. POLYTROPIC EFF. NOZZLE WEIGHT FL	OZ. WEIGHT FL OZ. WEIGHT FL
MENT PERFORMANCE RESULTS READING NUMBER 32 DA	INLET REL	1030.091	954.601	874.391	788.090	669.479	EXIT REL.	VELOCITY	695.264	624.265	514.544	506.357	490.844	INLET ARS	TANG, VEL	0	0.	0.	٠.	0.	TOT. TEMP	RATIO	1.11	1.101	1.102	1.096	1.098	UMENTATION A A G G G	WEIGHT FLOW/N Weight Flow/N
E	INLET REL	- 04 % O	0.8683	0.7986	0.7161	0.4063	EXIT REL.	MACH NO.	0.6034	0,5454	0.4499	0.4459	0.4349	CHJ		0.4514	0.4953	1.5155	0.5250	0.4120	TOT, PRESS	RATIO ,	1.371	1.358	1.336	1.352	1,368	ED INSTR	1.m. CHECK
BLADE NT NUMBER 12	INCID ANG	3001.304F	2.163	2.592	2.270	1.308	REL. TURN	ANGLE	13.129	14.053	17.762	27.593	43.96n	ST PRESS	RISE COEFF	n.38469	0.45257	0.49718	0.54986	0.93449	PCLYTROPIC	EFF1C1ENCY	0.8548	n.9082	0.8511	n.9433	0 9572	1.3580 0.8929 0.8975 n.980	
100	INCID ANG	N 1 . N 8 M . L N	6,913	8.302	R.840	8.588	REL. DEV.	ANG. T.F.	1.653	3.220	6.620	7.507	5.448	PIFFUSION	FACTOR	0.45A	0.479	0.558	0.509	0.447	ADIAPATIC	EFF ICIENCY	0.8482	n.9041	0.8449	0.940R	0.9552	PRESSURE RATIO = ANIAPATIC EFF. = POLYTROPIC EFF. = FICIENT L.F.	
	RFL INCET	. 695 - 95 567 - 569	62,303	60.552	58.550	59.188	HFL. FXIT	FLOW ANG.	58.12	4F.250	42.790	Э.	45.828															THAVEBSE PRESSURE RAT THAVERSE ADIAPATIC RE THAVEBSE POLYTROPIC E FLOW CCEFFICIENT L.F.	FLCW CCEFFICIENT PERCENT DESIGN SPEED
	RADIAL	101.100.	٠ م	m	4	'n	RADIAL	POSITION	**1	2	8	4	,Č	RADIAL	POSITION	-	2	8	4	ŗ.	RADIAL	POSITION		~	₩	4	ïν		

TOT, TEMP RATIO	1,112	1.096 1.091 1.093
TOT. PRESS RATIO	1,365 1,356	1,340 1,350 1,362
LOSS COEFFICIENT	0.1340	0,0788 0,0186 0,0067
ADIABATIC EFFICIENCY	0.8310 0.9197	0,9118 0,9819 0,9952
TOT. PRESS LOSS PARAM	0.0304	0.0175 0.0043 0.0015
RADIAL POSITION	1 2	m 4 s

Table 6, - Listing of Blade Element Performance (continued).

INLET AX. VELOCITY 696.702 670.988 660.808 629.106 516.399

AXI T REL 1 ANG. VEL 708.690 612.145 478.238 860.778 PEGS. FK PT 001. 002. 003. 003. 003. 003. A KIT A BBS CIT A 1.6210 0.9180 0.9234 212.89 0.99077 0.96487 INLET REL TANG. VEL 1201.157 1088.376 979.324 860.258 VELOCITY 658.732 671.090 664.092 643.763 VELOCITY 748.429 733.788 749.740 786.640 856.431 ABS.INLET FLOW ANG. 4/27/1967 CHOSTRUMENTATION PRESSURE RATIO ADIABATIC EFF.
POLYTROPIC EFF.
NOZZLE WEIGHT FLOW CHECK WEIGHT FLOW CHECK WEIGHT FLOW CHECK WEIGHT FLOW CHECK WEIGHT FLOW AT INLET 1201.157 1088.376 979.324 860.258 AT EXIT 11187.966 1088.998 991.441 892.373 EXIT ABS TANG.VEL 479.276 476.852 916.103 531.601 N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS 7 13 READING NUMBER 33 DAY INLET ABS TANG. VEL. 0. 0. INLET REL VELOCITY 1369.929 1278.642 1163.256 1074.465 VELDCITY 912.514 912.514 828.117 722.218 682.905 643.928 707. TEMP RATIO 1.188 1.170 1.173 1.157 1.158 FIXER INSTRUMENTATION EXIT REL. MACH NO. 0.7774 0.7119 0.6216 0.5558 TOT. PRESS 1.680 1.683 1.634 1.612 1.612 1.598 INLET REL MACH NO. 1.2676 1.1873 1.0991 0.9962 0.4723 0.5260 0.5602 0.5670 CH1 PCL YTROPIC EFFICIENCY 0.83n1 0.8967 0.9598 0.9365 81SE COEFF 0.37116 0.45027 0.51135 0.56206 0.53182 REL. TURN ANGLE 10.312 10.681 14.802 21.739 SUCT. SURF -1.217 -1.794 -1.970 -2.458 POINT NUMBER 1.6246 0.8719 0.8804 0.950 INCID ANG N.CMBR.LN 2.5933 7.956 3.740 3.930 AD1ABATIC FFFICIENCY 0.8177 0.8892 0.8506 0.9321 0.9080 THAVERSE PRESSURE RATIO
THAVERSE ADIABATIC EFF.
THAVERSE POLYTROPIC EFF.
FLOW CCEFFICIENT L.E.
FLOW CCEFFICIENT T.E.
PERCENT DESIGN SPEED ANG. T.F. 0.842 2.635 5.018 8.633 12.522 DIFFUSION FACTOR 0.462 0.477 0.523 0.500 KEL. EXIT FLOW ANG 51.022 47.665 41.188 32.083 18.302 FLOW ANG. 61.833. 61.833. 56.846 56.990 53.822 RABIAL POSITION RADIAL FOSITION RADIAL POSITION 1 2 3 4 RADIAL POSITION

40 B 4 B

VEL.RAT.O VEL.RAT.O 0.873 0.831 0.822 0.915

VELOCITY 573.439 557.703 557.703 543.082 575.508

TOT, TEMP RATIO	1,184	1,165	1,160	1,146	1,145
TOT, PRESS RATIO	1,636	1,644	1,617	1,608	1,586
LOSS COEFFICIENT	0.1470	0.0630	0.0711	0.0050	0.0350
ADIABATIC EFFICIENCY	0.8229	0.9252	0.9215	0.9949	0.9722
TOT, PRESS LOSS PARAM	0.0339	0.0142	0.0162	0.0011	0.0078
RADIAL POSITION		2	3	4	5

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK I (ROTOR 2D)

	INLET AX. VFLOCITY 651.915 663.216 641.862 602.307 493.573	EXIT AX. VFLOCITY 557.626 546.550 534.879 564.975	AXIAL VFL.RATIO 0.855 0.824 0.833 0.938		
	INLET ABS MACH NO. 0.605 0.516 0.598 0.571	EXIT ABS MACH NO. 0.645 0.633 0.651 0.687	EXIT REL TANG. VEL 673.285 592.535 456.536 346.371	FLOW ANG. FLOW ANG. 42.688 42.233 44.981 44.008	1.6460 0.9174 0.9230 19.41 0.99078
4/27/1967	INLET ABS VELOCITY 653.931 663.317 645.052 616.341 533.091	EXIT ABS VELOCITY 759.619 738.181 756.704 788.576	INLET REL TANG. VEL 1200.820 1088.070 979.049 860.017	ABS.INLET FLOW ANG. 0.00.00.00.00.00.00.00.00.00.00.00.00.	# 11 # 11 # # 25 *E *E C O
Ω ¥ ⊞	ROTOR SPD AT INLET 1200.820 1088.070 979.049 860.017	AT EXIT 1187.632 1088.692 991.063 892.122	EXIT ARS TANG. VEL 514.347 496.156 534.527 545.751 608.505	,	SURE RAT BATIC EF TROPIC E LE WEIGH WEIGHT
N.A.S.A. COMPRESSOR DUTPUT DATA BLADE ELEMENT PERFORMANCE RESULT 14 READING NUMBER 34 D	INLET REL VELOCITY 1367.331 1274.318 1172.446 1089.066	EXIT REL. VELOCITY 875.189 806.125 703.781 666.319	INLET ABS TANG. VEL 0. 0. 0.	101. TEMP RAF110 1.201 1.178 1.176 1.162	RUMENTATION WEIGHT FLOW WEIGHT FLOW
V.S.A. COMPRE DE ELEMENT PE TEADING	INLET REL 1.2656 1.1826 1.0865 0.9795	EXIT REL. MACH NO. 0.7428 0.6910 0.5904	0.4894 0.5424 0.5687 0.5706 0.4563	TOT, PRESS 148110 14841 1.664 1.643 1.631	FIXED INSTE
N.A BLAE INT NUMBER 1	INCID ANG SLCT. SURF -1.504 -1.209 -1.285	REL. TURN ANGLE 11.135 11.259 15.269 23.483	ST. PRESS RISE COEFF 0.38790 0.56772 0.56908 0.55909	PCLYTROPIC EFFICIENCY 0.8993 0.8755 0.9345	1.6514 10.8702 11.6514 11.6514 11.9514 11.9514
Cd	INCID ANG NN. CMBR.LN 2.723 3.246 4.501 5.235	REL DEV. ANG. T.E. 0.188 4.282 4.312 8.081	DIFFUSION FACTOR 0.497 0.539 0.539 0.516	AUTABATIC FFFICIENCY 0.88521 0.8821 0.8665 0.9298	PRESSURE RATIO ADIABATIC EFF. POLYTROPIC EFF. FFICIENT L.E. FFICIENT T.E.
	KFL. INLET 10. ANG. 54.503 57.536 56.751 56.753 56.733	• 3C P C + P			TRAVERSE PRESSUR TRAVERSE ADLATRO TRAVERSE POLYTRO FLOW CCEFFICIENT FLOW CCEFFICIENT FLOW CCEFFICIENT PERCENT DESIGN SPEEL
	RADIAL POSITIUN 1 2 3 4 4	PAADIAL POSITIUN 1 3 3 5 5	RADIAL POSITION 1 2 3 4 4 5	RAD LAL POSITIU:3 1 2 3 3 5 5	

RADIAL POSITION	TOT. PRESS LOSS PARAM	ADIABATIC EFFICIENCY	LOSS	TOT, PRESS RATIO	TOT. TEMP RATIO
	0,0356	0.8233	0.1522	1,671	1,192
	0,0153	0,9230	0,0675	1,675	1,172
	0,0156	0,9283	0.0677	1,646	1,165
	0,0021	0.9910	0,0092	1,622	1,150
	0,0089	0.9694	0.0401	1,596	1.148

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK I (ROTOR 2D)

	INLET AX. VFLOCITY A31.507 648.168 A36.819 604.550	EXIT AX VFLOCITY 545.290 533.882 560.162 560.462	7
	INLET ABS MACH ABS 0.585 0.593 0.593 0.573	MACH NO. 0.653 0.653 0.647 0.731 EXIT REL	24 253 357 357 357 357 357 357 357 357 357 3
	INLET ABS VELNCITY 633.460 648.267 639.983 618.636	EXIT ABS VELOCITY 771.858 741.357 753.186 771.545 834.848	12505 1200.050 1200.0
, T T	ROTOR SPD 'AT INLET 1200.364 1087.657 978.677 859.690 724.276	ROTOR SPD AT EXIT 1187.181 1088.278 990.686 891.783 794.813	VEL TANG VEL 1. 544.948 514.383 542.113 540.969 604.173 TEMP 10 PRESSURE RATIO ADIABATIC EFF NOZZE WEIGHT FLOW FLOW/NDZ. WEIGHT FLOW
N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULT: 15 RFADING NUMBER 35 D	INLET RFL VELOCITY 1357.256 1266.194 1169.354 1059.140 895.328	EXIT REL. VELOCITY 843.361 783.821 688.927 652.461 606.868	992 TANG. VEL T 992 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.
A.S.A. COMPRE DE ELEMENT PE 5 RFADING	INLET REL MACH NO. 1.2532 1.1746 1.0834 0.9802	EXIT REL. MACH NO. 0.7136 0.5920 0.5668 0.516	0.4992 0.5916 0.5988 0.5988 0.4885 107. PRESS RATIO 1.731 1.648 1.648 1.633 1.643 1.643 1.643 1.643 1.643
NT NUMBER	INCID ANG SLCT. SURF -0.299 -0.932 -1.012 -1.396	ANGLE 12.584 12.138 16.283 22.164 37.280	RISE COEFF 0.44772 0.59854 0.59861 0.59861 0.58877 0.8877 0.9373 0.9373 0.9373 0.9373 0.9373 0.9373 0.9373
104	INCID ANG MN.CMBR.LN 3.471 3.818 4.698 5.174	AREL DEV. ANG. 1.F0.513 2.040 4.495 9.270 13.006	FACTOR 0.525 0.526 0.527 0.524 0.487 0.487 0.487 0.8042 0.8042 0.8042 0.8042 0.8042 0.8728 0.9274 0.9274 PRESSUME HATIO = POLYTROPIC FFF. =
	FEI. INLET FLOW ANG. 60.201 59.208 56.948 54.884 56.056	KFL. EXIT FLON ANG. 49.667 47.070 40.665 32.720 18.786	FACTO 0.52 0.52 0.52 0.54 0.55 0.68 0.48 FFICI 0.80 0.80 0.80 0.80 0.80 0.82 ELCHAVERSE PRESSUME HA THAVERSE POLYTROPIC FLCM CCEFFICIENT L.E FLCM CCEFFICIENT L.E PERCENT DESIGN SPEED
	RADIAL POSITION 1 2 3 4 5	RADIAL POSITION 1 2 3 3 4 5 8 8 DIAL	POSITION 1 2 3 3 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5

	TOT. TEMP RATIO	1,198	1,176	1,167	1, 151	1,149
I NOT THE TOTAL	TOT. PRESS RATIO	1.684	1,693	1,660	1.629	1.607
THE PROPERTY OF THE PARTY OF	LOSS COEFFICIENT	0,1660	0.0724	0.0663	0.0076	0,0339
INVESTERS DETERMINED INCH LAKE INSTRUMENTALION	ADIABATIC EFFICIENCY	0,8133	0,9197	0.9310	0.9926	0.9747
Tolly 1	TOT. PRESS LOSS PARAM	0.0394	0.0165	0.0152	0.0017	0.0075
	RADIAL POSITION	1	2	3	4	5

Table 6. - Listing of Blade Element Performance (continued).

N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS > POINT NUMBER 16 RFADING NUMBER 36 DATE 4/27/1967

	INLET AX. VFLOCITY 792.510 788.086 760.294	586.228 EXIT AX. VFLOCITY R75.354 785.559 644.750	887,188	AXIAL VFL.RATIO 1.105 0.997 0.848		
	INLET ABS MACH NO. 0.749 0.743	0.587 EXIT ARS HACH NO. 0.051	1.060	EXIT REL 1166.233 1022.518 813.186	ABS.EXIT FLOW ANG. 18.063 21.426 31.703	.4400 .7455 .7582 .90
	INLET ARS VELOCITY 794.961 788.206 764.072	633.164 EXIT ABS VELOCITY 922.766 843.906 758.587	1167.781	INLET REL 1467.844 1330.023 1196.759	ABS.INLET FLOW ANG. 0. 0. 0.	2 0 0 3 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	ROTOR SPD AT INLET 1467.844 1330.023 1196.759	885.669 ROTOR SPD AT EXIT 1451.724 1330.782 1211.444	971.923	EXIT ABS TANG.VEL 285.491 308.264 398.258		NUMENTATION PRESSURE RATIO ADIABATIC EFF. POLYTROPIC EFF. NOZZLE WEIGHT FLOW WEIGHT FLOW/NOZ. WEIGHT FLOW WEIGHT FLOW/NOZ. WEIGHT FLOW
•	INLET REL VELOCITY 1669.290 1546.036 1419.872	1088.718 EXIT REL. VELOCITY 1459.483 1289.455 1038.324	943.728	INLET ABS TANG. VEL 0. 0.	101. TEMP RATIO 1.122 1.126 1.141	JMENTATION PR PC PC WEIGHT FLOW/NC
	INLET REL MACH NO. 1.5718 1.4573	1.0089 EXIT PEL. MACH NO. 1.3126 1.1468	0.8570	CH1 0.1451 0.2091 0.2170	101, PRESS RATIO 1.343 1.358 1.262	FIXED INSTRUMENTATION L.E. CHECK WEIGHT FLO T.E. CHECK WEIGHT FLO
,	INCID ANG SLCT. SURF -0.915 -0.788	7.381 ANGLE 8.526 6.885	41.207	ST. PRFSS RISF COEFF 0.07800 0.14218 0.17011	POLYTROPIC EFFICIENCY 0.7340 0.7373 0.5030	
•	INCID ANG MN.CMBR.LN 2.455 3.962 5.322	5.899 PEL. DEV. ANG. T.E. 2.929 7.436 15.420	9.513	DIFFUSION FACTOR 0.188 0.233 0.354	ADIAHATIC FFFICIENCY 0.7256 0.7257 0.4865	
	MEL. INLET FI OK ANG. 61.635 59.352 57.572	AFL. EXIT FLOW ANG. 53.109 57.500	15.243			THAVERSE ADIABATIC EFF. THAVERSE ADIABATIC EFF. THAVERSE POLYTROPIC EFF ELOW CCEFFICIENT L.E. FLCW CCEFFICIENT T.E. PERCENT DESIGN SPEED
	RADIAL POSITIUN 1 2	SADIAL POSITION 1 2 3	æ	RADIAL POSITION 1 2 3	RADIAL POSITIUN 1 2 3 3	

TOT. TEMP RATIO	1,116 1,133 1,134	1,197
TOT. PRESS RATIO	1,322 1,361 1,269	1.712
LOSS	0.1279 0.1691 0.2825	0.1974
ADIABATIC EFFICIENCY	0.7182 0.6937 0.5261	0.8438
TOT. PRESS LOSS PARAM	0.0282 0.0345 0.0532	0.0446
RADIAL POSITION	3 2 1	5

Table 6. - Listing of Blade Element Performance (continued).

	INLET AX. VFLOCITY 786.861 785.899 765.040 726.824 590.986	EXIT AX. VFLOCITY 757.875 726.966 549.642 803.199	AXIAL VFL.RATIO 0.963 0.925 0.718 1.105	
	INLET ABS MACH NO. 0,743 0,741 0,724 0,592	MACH NO. 0.7745 0.7745 0.0774 0.080	EXIT REL 7 ANG. VEL 907.581 795.450 379.581 201.624 201.624 ABS. EXIT FLOH ANG. 35.446 46.755 42.141	1,748 0,7944 0,8099 3,91 0,98593 1,03303
4/27/1967	INLET ARS VELNCITY 789.294 786.019 768.841 743.758	EXIT ABS VELOCITY 935.476 903.741 802.780 1077.985	INLET REL 1469.550 1331.569 1198.150 1052.479 886.699 ABS. INLET FLOW ANG. 0.	4 H H H H H H A 3 3 3 3 3 3 3 3 3 3 3 3 3
ñ	ROTOR SPD AT INLET 1469.550 1331.569 1198.150 1052.479 886.699	ROTOR SPD AT EXIT 1453.412 1332.329 1212.852 1091.770 973.053	EXIT APS TANG.VFL 545.831 536.870 564.397 712.178 771.479	SURE RAY BATIC EF TROPIC E LE WEIGHT WEIGHT
N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS 17 READING NUMBER 37 DA	INLET REL VELOCITY 1668.102 1546.254 1423.615 1288.755 1092.550	EXIT REL. VELOCITY 1183.590 1077.625 835.399 893.837	TANG. VFL 0. 0. 0. 0. 0. 1.223 1.223 1.223 1.225 1.225	UMENTATION PRES ADIA POLY NOZZ WEIGHT FLOW/NOZ.
A.S.A. COMPRES DE ELEMENT PES PEADING	INLET REL MACH NO. 1.5698 1.4569 1.3410 1.2102	EXIT REL. MACH NO. 1.0055 0.9230 0.7075 0.838	CH1 0.3413 0.3986 0.4088 0.3240 0.7240 1.764 1.766 1.786 1.786 1.786	FIXED INSTRUMENTATION L.E. CHECK WEIGHT FLO T.E. CHECK WEIGHT FLO
NT NUMBER	INCID ANG SLCT. SURF -0.717 -0.689 -0.519 -0.908	REL. TURN ANGLF 11.697 11.875 8.614 30.076 43.011	ST. PRESS RISE COEFF 0.22210 0.33542 0.33542 0.33542 0.33542 0.17343 0.17343 0.17365 0.6488 0.6488 0.6488	= 1.767n = 0.7635 = 0.7816 = 0.7816 = 0.980 = 1.0950
110d	INCID ANG MN. CPBR.LN 3.053 4.063 5.191 5.662	WEL. DFV. anG. T.E. an. 12.657 12.657 1.845 7.526	PIFFUSION FACTOR 0.410 0.538 0.538 0.458 0.350 ablakatic APIAKATIC APIAKATIC 0.8111 0.8247	0 • 14
	HFI. INLET FLOW ANG. 61.23 59.451 57.441 55.372 56.316	HEL. EXIT FLOR ANG. A7.536 A8.827 A8.827 JR.295		THAVERSE PRESSURE RAT THAVERSE ADIARATIC EF THAVERSE POLYTROPIC EI FLCW CCEFFICIENT L.E. FLCW CCEFFICIENT T.E. PERCENT DESIGN SPEED
	RADIAL POSITION 2 3 3	AADTAL POSITION 1 2 3 5 5 5	RADIAL POSIȚIUN 2 3 3 4 5 5 POSITIUN 1	

PARAMETERS DETERMINED FROM FIXED INSTRUMENTATION

	ADIABATIC LOSS TOT. PRESS TO' EFFICIENCY COEFFICIENT RATIO	0.7124	0,7872 0,1824 1,762	0.7157 0.2444 1.609	0.8771 0.1281 1.812	0.8953 0.1624 1.867
Nu 1	TOT. PRESS LOSS PARAM	0.0544	0,0412	0.0487	0,0313	0.032
	RADIAL POSITION	-	2	٣	7	ď

Table 6. - Listing of Blade Element Performance (continued)

AXIAL VEL.RATIO 0.933 0.895 0.738 1.025 EXIT AX. VFLOCITY 732.383 702.051 558.403 736.871 INLET AX. VELOCITY 784.659 784.774 756.488 719.000 584.613 EXIT REL TANG.VEL 864.313 751.337 763.880 347.796 INLET A8S HACH NO. 0.741 0.745 0.691 0.586 HACH NO. 0.789 0.773 0.773 0.722 0.911 ABS.EXIT FLOW ANG 38.716 39.520 49.216 45.217 44.359 233.84 0.98436 1.03716 1,829 0,8099 0,8253 EXIT ABS VELNCITY 940.041 910.123 855.370 1049.960 INLET REL 1467.515 1329.725 1196.491 1051.022 885.471 1NLET ABS VELOCITY 787.085 784.893 760.247 735.752 631.420 ABS.INLET FLOW ANG. 0. 0. 0. DATE 4/27/1967 ADIABATIC EFF.
POLYTROPIC EFF.
NOZZLE WEIGHT FLOW
L.E. CHFCK WEIGHT FLOW/NOZ. WEIGHT FLOW
T.E. CHECK WEIGHT FLOW/NOZ. WEIGHT FLOW PRESSURE RATIO AT INLET 1467.515 1329.725 1196.491 1051.022 885.471 AT EXIT 1451.399 1330.484 1211.173 1090.258 971.706 EXIT ARS TANG.VEL 587.086 579.147 647.292 742.462 N.A.S.A. COMPRESSOR OUTPUT DATA RLADE ELEMENT PERFORMANCE RESULTS R 18 RFADING NUMBER 38 DAT EXIT REL. VELOCITY 1134.038 1028.310 794.123 819.833 1NLET ARS TANG. VEL 0. 0. 0. 101. TEMP RATIO 1.276 1.245 1.247 1.249 INLET REL VELOCITY 1665.264 1544.094 1417.591 1282.957 1087.543 FIXED INSTRUMENTATION 101, PRESS RAIIC 1.940 1.730 1.924 1.924 EXIT REL. MACH NO. 6.9517 0.8738 0.6703 0.7111 IMLET MEL MACH NO. 1.5472 1.4564 1.3440 1.9949 0,3803 0,4357 0,4529 0,4066 0,2358 CHI RISE COEFF 0.25487 0.33297 0.33891 0.318001 0.31806 POLYTROPIC EFFICIENCY 0.7275 0.8197 0.7108 0.8417 SUCT. SUPF -0.68% -0.68% -0.68% -1.36% -1.314 REL. TURN ANGLE 12.144 32.510 32.417 30.357 1,8579 10,7690 10,7882 10,980 110,950 POINT NUMBER 1NCIB ANG NN.CMBR.LN 3.487 4.662 5.447 5.914 5.966 ADJAHATIC FFFICIENCY 0.7029 0.8828 0.6878 0.8558 PEL. DEV. ANG. T.E. -0.457 1.912 9.110 1.817 FACTOR 0.448 0.579 0.579 0.579 0.579 THAVERSE PRESSURE RATIO THAVERSE ADIAHATIC EFF. THAVERSE POLYTROPIC EFF. FLOW CCEFFICIENT L.E. FLOW CCEFFICIENT T.E. PERCENT DESIGN SPEED HEN, EXIT HEN, ANG. 46,942 46,948 45,280 ## 1. INLET # 1. EAN # 1. EAN # 2. 452 # 7. 697 # 7. 697 # 55. 624 RADIAL POSITIUN RABIAL POSITION RADIAL POSITION 1 2 3 3 5 RADIAL POSITION

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11 C 10 7 L

TOT, TEMP RATIO	1.258	1,237	1.224	1,223	1,217
TOT, PRESS RATIO	1,791	1,850	1,739	1.872	1.900
LOSS COEFFICIENT	0.2571	0.1711	0.2208	0,1325	0,0996
ADIABATIC EFFICIENCY	0.7027	0.8106	0,7651	0.8790	0.9284
TOT. PRESS LOSS PARAM	0.0610	0.0391	0.0471	0.0324	0.0225
ADIAL SITION		7	3	7	2

Table 6. - Listing of Blade Element Performance (continued).

NASA - TASK I (ROTOR 20)

		٥	N,A,S, BLADE B POINT NUMBER 19	S.A. COMPRESE FLEMENT PPF	S.A. COMPRESSOR OUTPUT DATA FLEMENT PERFORMANCE RESULTS READING NUMBER 39 DA	œ ⊨	4/27/1967		
RADIAL	RELINLET	INCID ANG	INCID ANG	INLET REL	INLET REL	ROTOR SPD	INLET ABS	INLET ABS	INLET AX
201-10	A0.150	3.372	86E.E.	.0420	1661.462	1468.060	777.981	0.731	775.583
٠, ٠	59.657	4.257	-0.483	1,4524	1541,414	1330,218	778.767	0.734	778.648
· * 5	57.518	5.26R	-0.442	1.3378	1420.945	1196.935	765.788	0.721	762.002
4	55.740	5,530	-1.040	1.2124	1289.569	1051.412	746.673	0.702	729.672
5	54.232	5.632	-1.64R	1.0139	1092.641	885.799	639.706	0.594	592.285
2 A 13 I A L	7. EX. T	REL. DEV.	REI TURN	EXIT REL.	EXIT REL.	ROTOR SPD	EXIT ABS	EXIT ARS	EXIT AX.
7011-903	10 10 14 10 14 16 14 16 14 16 14 16 14 16 14 16 14 16 14 16 14 16 16 16 16 16 16 16 16 16 16 16 16 16	1 L C V	T I I I	MACH	VELOCITY	EXIT	VELOCITY	MACH NO.	VFLOCITY
	49.378	-1. An2	13.774	0.8893	1067,684	1451,938	965.855	0.804	708.408
· ^	47,173	2,143	12,484	D. A252	978,539	1330.978	904.799	0.763	665,184
, - ~	45.326	9.156	12.192	0.6387	760.145	1211.622	858.399	0.721	534.076
4	95,653	2.203	29.586	0.6712	780.112	1090.663	1032.421	0.888	698.949
ın	14,364	10.584	39.867	0.6860	784.995	972.066	1068.624	0.934	734.256
0 4 0 1 4 5		NOTSUBSTG	ST PRESS	Ę.	SA THE INT	EXIT ABS	IN PR	FXIT REL	AXIAL
2011-000		FALTOR	RISE COEFF		TANG. VEL	TANG. VEL	TANG. VEL	TANG. VEL	VFL . RAT I
		0.501	0.27122	0.3988	0	654.659	1468.060	797.278	0.913
• ~		0.498	0.35917	0.4641	•	613,318	1330.218	717,660	0.854
) (~ ?		0.609	0.41894	0.4951	0	671.437	1196.935	540.185	0.701
4		0.556	0.44739	0.4761		754.983	1051.412	335.680	0.958
۳.		0.451	n.42680	0.3503	· c	756.458	885.799	215.609	1.240
9 A D 1 A L		ADJABATIC	n.	TOT, PRESS	TOT. TEMP		ABS.INLET	ABS, EXIT	
P01:1804		FFF 10 JENCY	EFF 1C1ENC	PATIO	RAT10		FLOW ANG.	FLOW ANG.	
1		0.6896		1.048	1.304			42,742	
~		0.7916	8608.0	1.924	1.260		0	42.677	
8		0.7142	n,7368	1.804	1.257		0.	51,500	
4		0.4359	0.8509	1.989	1.260		0.	47.207	
5		0.8659	0.8777	1.924	1.239		ċ	45.853	
	TABVERSE PRETABLE POL	PRESSURE RATIO ADIAHATIC EFF. POLYTROPIC FFF.	= 1.9227 = n.7694 = n.7895	FIXEN INSTRUMENTATION	UMENTATION	PRESSURE RATIO ADIABATIC EFF. POLYTROPIC FFF	4 M 44	1.8890 0.8138 0.8297	
	FLOW COEFFICIENT L.F. FLOW COEFFICIENT T.E.	CIENT L.F. Cleut T.F.	-	CHECK		NOZZLF WEIGHT FLOW FLOW/NOZ, WEIGHT FLOW	233.1	.13 .98826	
	PERCENT DESIGN SPEED	SFEED		I.E. CHECK	MEIGH! FLUW/	FLUM/NUZ. WEIGHI FL	1.0	2123	

TOT, TEMP RATIO	1,278	1,252	1,236	1,232	1,220
TOT, PRESS RATIO	1,882	1,920	1.808	1.901	1,930
LOSS COEFFICIENT	0.2645	0,1756	0.2157	0.1451	0.0861
ADIABATIC EFFICIENCY	0,7120	0,8149	0.7802	0.8702	0.9386
TOT. PRESS LOSS PARAM	0.0645	0.0399	0.0460	0.0354	0.0193
RADIAL POSITION	1	2	٣	7	٠,-

Table 6. - Listing of Blade Element Performance (continued).

N.A.S.A. COMPRESSOR OUTPUT DATA BLADE ELEMENT PERFORMANCE RESULTS POINT NUMBER 20 READING NUMBER 40 DATE '4/27/1967

INLET AX.						583,896	EXIT AX.	×1100	703,706	658,180	531,591	704,426	732.453	AX I AL	VFL.RAT10	906'0	0.845	0.705	0.984	1.254									
INLET ABS	MACH NO.	0.732	0.734	0.713	0.688	0.584	EXIT ABS	2	0.805	0.764	0.725	0.896	0.937	EXIT REL	TANG.VFL	783,335	704.662	530.150	328.0A5	207.190	ABS.EXIT	FLOW ANG.	43.489	43.534	52.007	47.240	46.214	1.908 0.8128 0.8290 2.99	.02609
INLET ABS	VELOCITY	. 779.279	779.062	758.051	732.580	630.646	FX1T ABS	× 1 0 0 1 1 1 1	971.193	907.893	864.029	1041.148	1072.787	INLET REL	TANG, VFL	1466.971	1329.232	1196.047	1050.632	885.143	ABS, INLET	FLOW ANG.	.0	· •	0.	٠.	٥.	M; Cs - 11 11 11 11 11 - 32	. 11
 ROTOR SPD	AT INLET	1466.971	1329.232	1196.047	1050.632	885.143	ROTOR SPD	F - > U - F -	1450.861	1329,991	1210.724	1089.854	971.346	EXIT ARS	TANG. VFL	667.527	625,329	680.574	761.769	764.156								UMENTATION PPESSURE RATIO ADIABATIC EFF. POLYTROPIC FFF. NOZZLE WEIGHT FLO	JOZ. WEIGHT FL
INLET REL	VELOCITY	1661.108	1540.713	1416.041	1280,821	1086.826	EXT PE		1054.152	964.252	751.282	781.880	780.938	INLET ARS	TANG, VEL					÷.	TOT. TEMP	RATIO	1.313	1.265	1.262	1.263	1.239	UMENTATION P	WEIGHT FLOW/N
INLET REI.	MACH NO.	1,5613	1.4517	1.3322	1.2021	1.0071	FXT		0.8743	0.8115	0.6307	0.6729	0.6824	CH 3		0.4097	0.4733	0.4998	9.4717	0.3505	TOT, PRESS	RATIO	1.980	1.946	1.824	2.009	1.943	S	T.E. CHECK
INCID ANG	SUCT, SURF	-4.455	-0.511	-0.19B	-0.550	-1.291	2001		14 030	12.676	12.84	30 756	40.794	ST, PRESS	RISE COEFF	n. 28080	0.36812	0.42445	n.44473	0.42889	PCI YTROPIC	EFFICIENCY	0.7175	0.8089	0.7399	9.8556	0.8863	1.0455 0.7714 0.7917 0.980	110
INCID ANG	MN.CMBR.LN	3,315	4.239	5.512	6.020	5.989	7 11 4		ANG. 1-17.	1.02	8.75.2	1.524	10.015	PIFFUSION	F.A.C.TOR	0.512	0.510	0.616	0.553	0.453	2DIARATIC	FFF 1C LENCY	0.6895	5062.0	0.7171	0.5408	0.4752	PPESSURE RATIO APLANATIC FFF. FICEMULY.	SPEED
HEL.INLET	FLOW ANG.	42.095	59.629	57.762	55.730	54.589	# F			26.5.3	66.84	24 974	46.795															TKAVERSE PRESSURE RAT TAAVERSE ANTAHATIC EF TRAVERSE POLYTROPIC E FLOG COEFFICIANT LE	PERCENT DESIGN SPEED
RADIAL	POSITION		۰ ۸	; M.	4	ī	0 4 0	1 - H	50111507	+ 0	. ~	9	ۍ.	RADIAL	POST102		٠, ٨	; ~	- 4	5	RADIAL	VOITISON		C.	~	4	ľ		

TOT, TEMP RATIO	1.285	1.257	1.241	1,235	1,222
TOT. PRESS RATIO	1.910	1.947	1.829	1,909	1,939
LOSS COEFFICIENT	0.2696	0,1766	0.2187	0,1538	0.0885
ADIABATIC EFFICIENCY	0.7119	0.8169	0,7813	0.8649	0.9379
TOT. PRESS LOSS PARAM	0,0661	0.0403	0.0469	0.0377	0.0199
RADIAL POSITION	-1	2	3	~ †	5

Table 6. - Listing of Blade Element Performance (continued).

N.A.S.A. COMPRESSOR OUTPUT DATA
BLADE FLEMENT PERFORMANCE RESULTS
POINT NUMHER 21 READING NUMBER 41 DATE 4/27/196

	INLET AX.	VFLOCITY	765.516	774.731	759.861	724.643	592,311	FXIT AX.	*T100 137	679 707	651,917	510.170	684.188	710.887	AXTAI	VEL RATIO	0.888	0.841	0.683	0.944	1.200										
	INLET ABS	MACH NO.	0.720	0.730	0,719	0.697	0.594	EXTT ABS	Z TOVE	0.803	0,769	0.722	468.0	0.916	EXIT REL	TANG. VEL	757.413	688.777	524.848	325,360	215.313	A 1 A 2 3 G 7	FI OW ANG.	45.624	44.576	52.917	48.207	46.794	320 131	296 6	0.98889 1.01407
4/27/1967	INLET ARS	VELOCITY	767.884	774.849	763.637	741.526	639.734	EXIT ABS	VELOCITY	973.061	915.225	861.468	1030.069	1052.083	IN FR	TANG. VEL	1468.221	1330.364	1197.066	1051.527	885.896	TO WE OUT	FLOW ANG.	•	0	· c	0.	0.			U H
DATE 4/27,	ROTOR SPI	AIINLFT	1468.221	1330.364	1197.066	1051.527	885.896	ROTOR SPD	AT EXIT	1452.097	1331,124	1211,755	1090.782	972.173	EXIT APS	TANG, VEL	694.684	642.347	686.907	765.422	756.860								PRESSURE RATIO ADIABATIC EFF.	OLYTROPIC EFF. Ozzle Weight F	FLOW/NOZ. WEIGHT FLOW FLOW/NOZ. WEIGHT FLOW
NUMBER 41	INCET REL	VELUCITY	1656.900	1539.565	1419,897	1286.690	1092.736	EXIT REL.	VELOCITY	1018,791	948.389	738.751	762.253	761.841	INLET ARS	TANG. VEL	٥.	0.			0.	TOT TEMP	RATIO	1.323	1.272	1.264	1.265	1.241		άŽ	WEIGHT FLOW/N
I READING	INLET REL	APCIL SO.	1.555	1.4495	1,3361	1.2087	1.0141	EXIT REL.	MACH NO.	0.8408	9.7964	0.6190	0.6539	0.6633	Сн1		0.4147	0.4830	0.5189	0.5036	0.3981	TOT PRESS	RATIO	2,000	1,983	1.852	2,032	1.951	FIXED INSTRUMENTATION		L.E. CHECK T.E. CHECK
INT NUMBER 21	INCID ANG	3.00.13.00	/w0.n-	-0.354	-n.366	-0.852	-1.647	REL. TURN	ANGLF	14.368	13.211	12.283	26.66	39.383	ST, PRESS	RISE COEFF	n.28591	0.37773	0.44316	n.47597	п.47451	PCI YTROPIC	EFFICIENCY	n.7084	9.8129	0.7525	n.8612	ი.8859	= 1.969n = 0.7724	= 0.7929 = n.980	= 0.950 = 110
104	TNCTP ANG	21. KAII. ME	SX0.0	4.396	5.344	5.718	5,633	PFL. DEV.	ANG. T.F.	-2.085	1.545	9.141	1.983	11.070	PIFFUSION	FACTOR	0.538	0.524	0.627	0.571	0.472	ADIARATIC	FFF 1 C1ENCY	0.6790	0.7942	0.7303	0. x46A	0.8747		! !	
	MFT. INLET	SINE STATE	00.00	. / S.A.	57.594	55.428	56,233	MFL. FXIT	FIDS ANG.	44.095	44.575	45.311	25.433	14.850															THAVERSE PPE	PLOW CCEPFICIENT L.E.	FLCW CCEFFICIENT PERCENT DESIGN SPEED
	RADIAL			~	~	4	'n	RADIAL	FOSITION		~	~)	4	ĸ	HADIAL	POSITION		~	m	4	ľ	RADIAL	POSITION	1	~	8	4	2			

TOT, TEMP RATIO	1,293	1,263	1,246	1,238	1,224
TOT. PRESS RATIO	1.943	1,981	1.855	1,922	1,950
LOSS COEFFICIENT	0.2756	0.1776	0.2199	0.1556	0.0895
ADIABATIC EFFICIENCY	0.7125	0.8196	0.7833	0.8638	0.9372
TOT. PRESS LOSS PARAM	0.0675	0.0409	0.0469	0.0380	0.0200
RADIAL POSITION		2	3	7	5

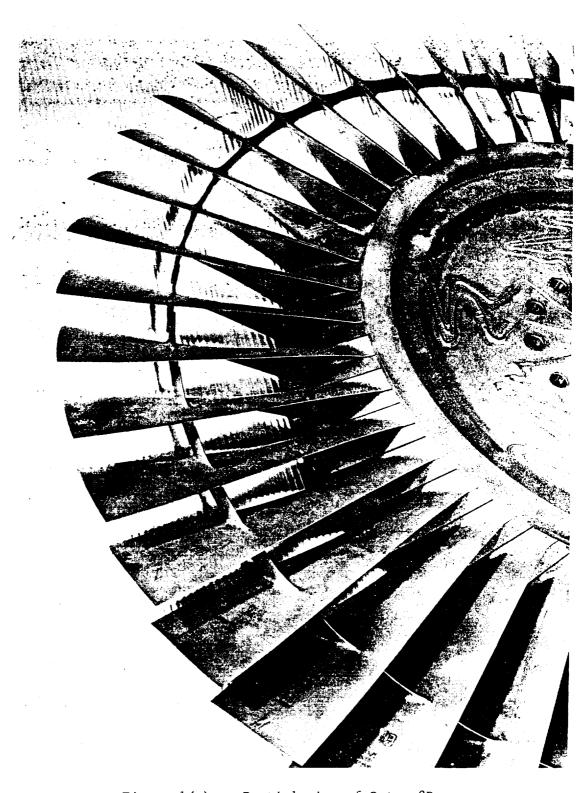


Figure 1(a). - Partial view of Rotor 2D.

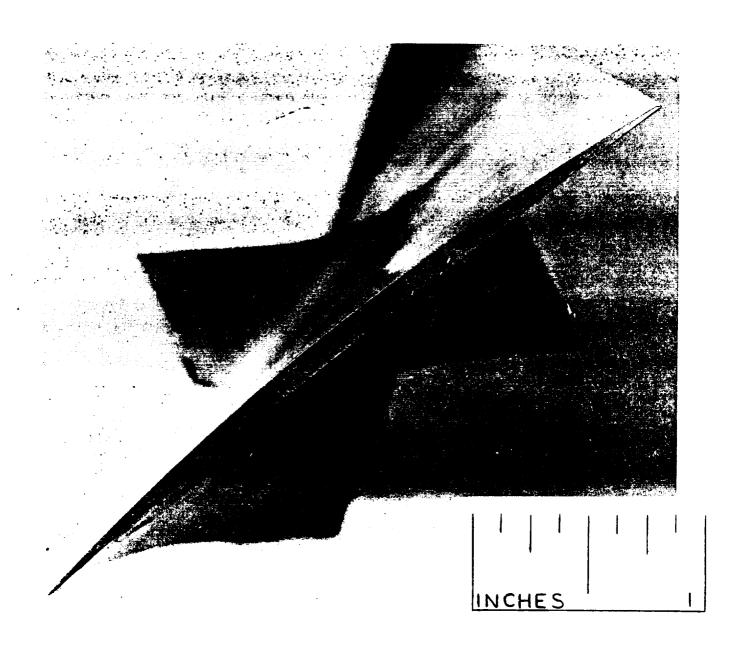


Figure 1(b). - Close-up view of tip section of Rotor 2D.

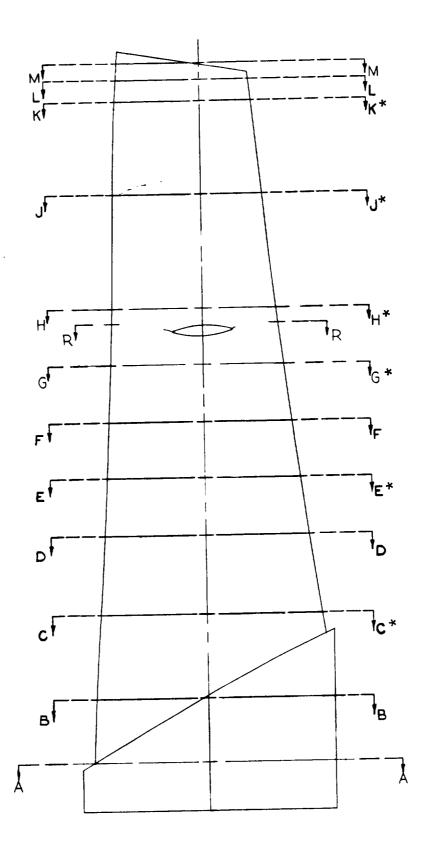


Figure 2. - Meridional view of rotor. Probograph inspection sections are indicated by asterisks.

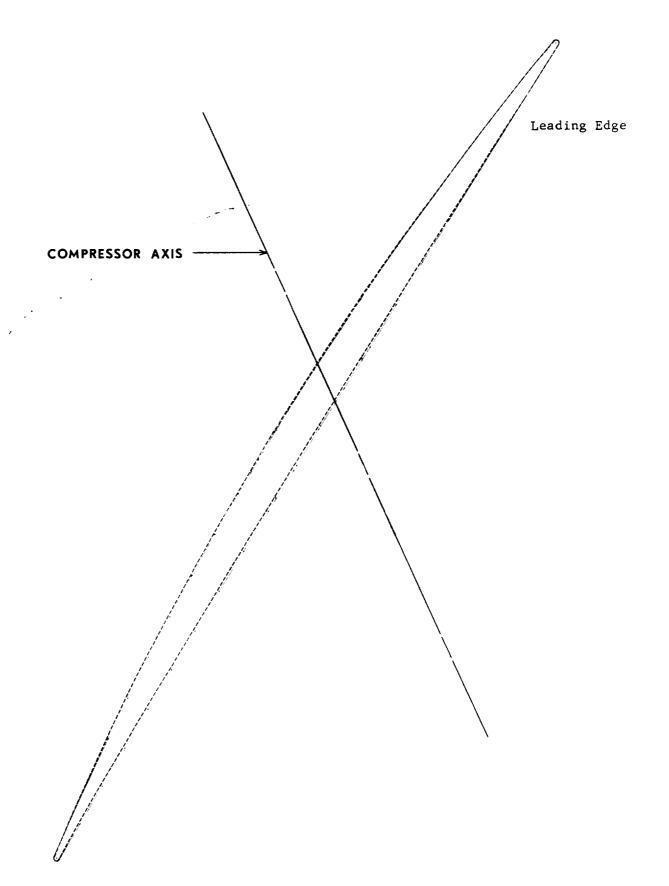


Figure 3(a). - Cylindrical cut of blade at section KK. The solid line represents design intent and the dashed line represents the average of six measured samples.

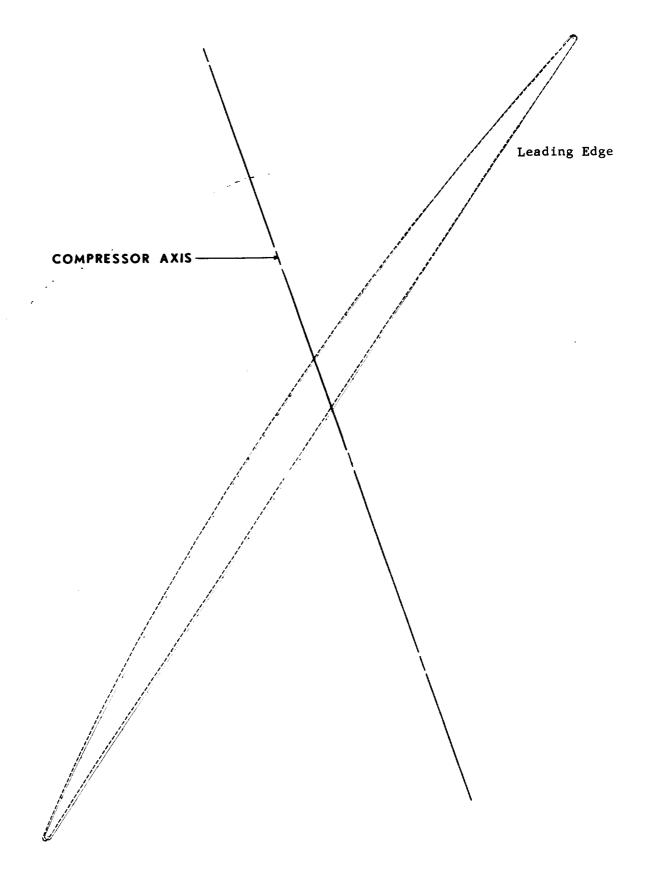


Figure 3(b). - Cylindrical cut of blade at section JJ. The solid line represents design intent and the dashed line represents the average of six measured samples.

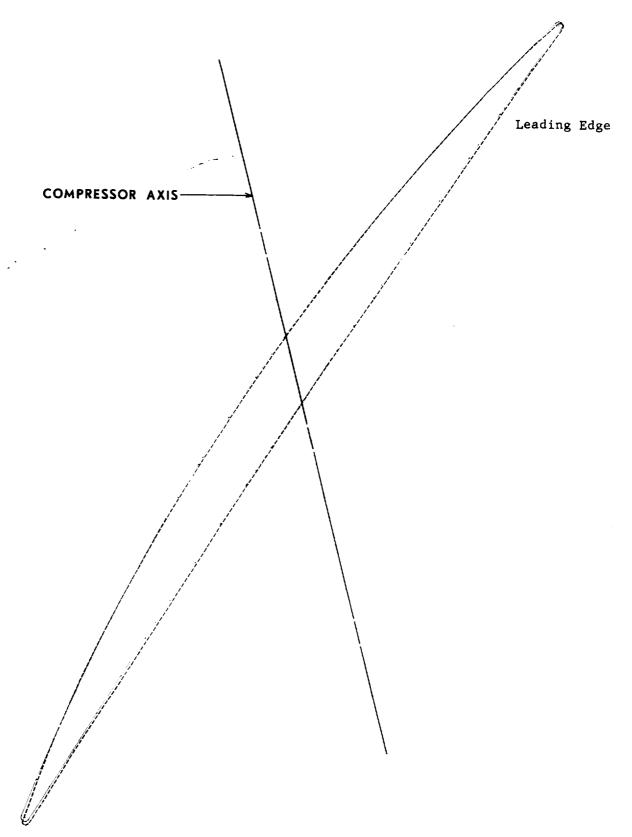


Figure 3(c). - Cylindrical cut of blade at section HH. The solid line represents design intent and the dashed line represents the average of six measured samples.

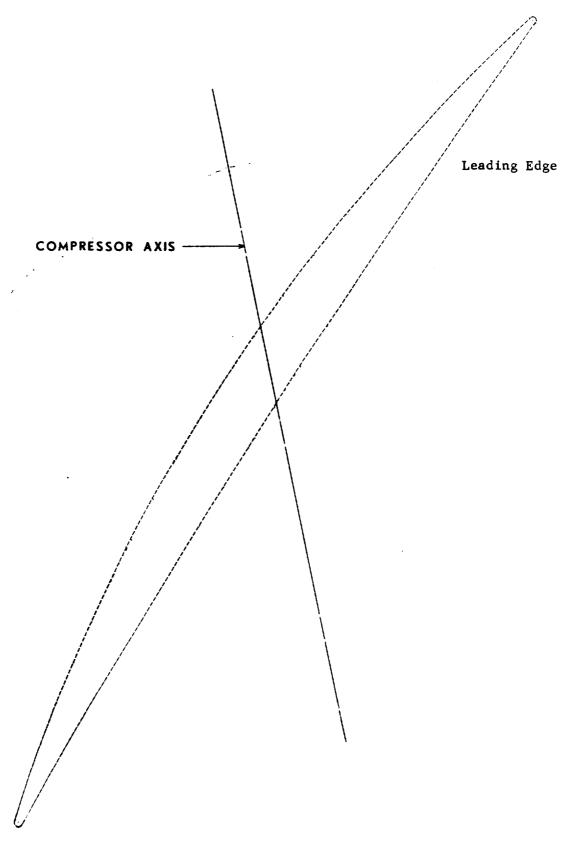


Figure 3(d). - Cylindrical cut of blade at section GG. The solid line represents design intent and the dashed line represents the average of six measured samples.

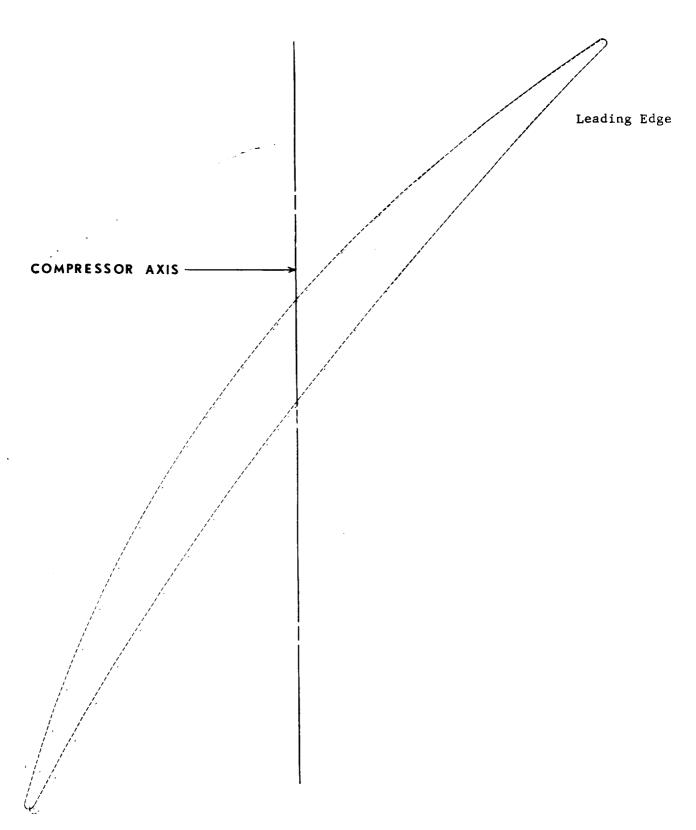


Figure 3(e). - Cylindrical cut of blade at section EE. The solid line represents design intent and the dashed line represents the average of six measured samples.

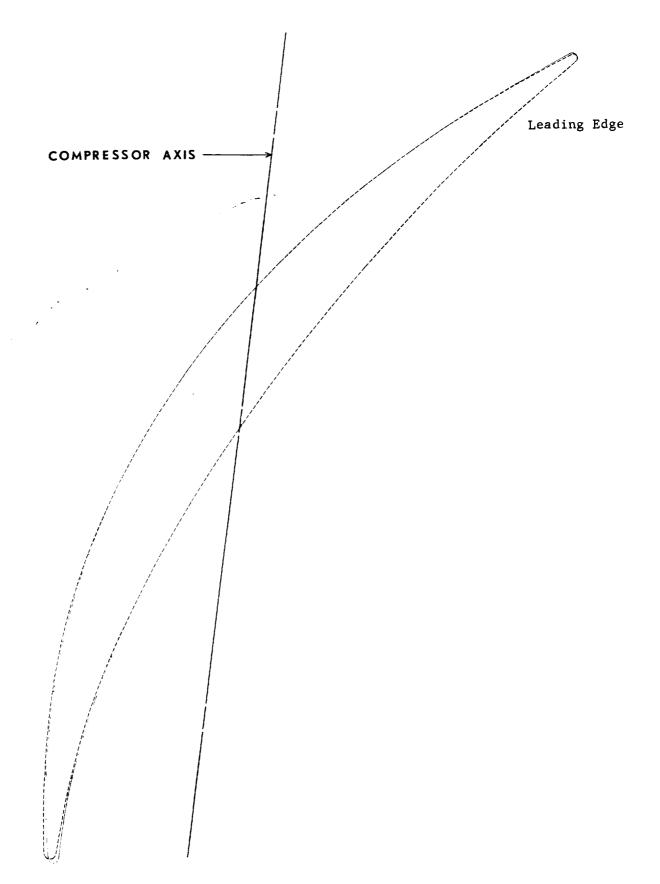


Figure 3(f). - Cylindrical cut of blade at section CC. The solid line represents design intent and the dashed line represents the average of six measured samples.

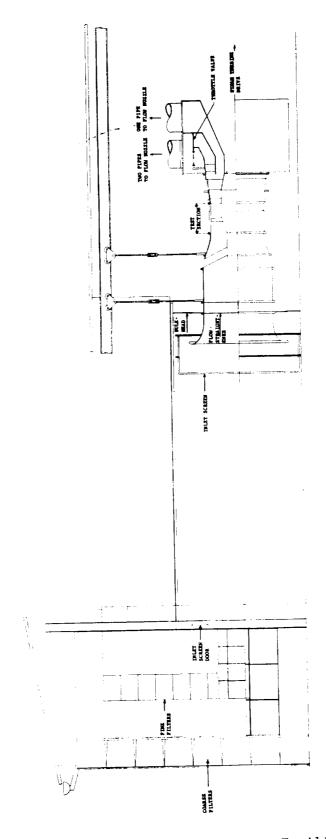


Figure 4. - House Compressor Test Facility.

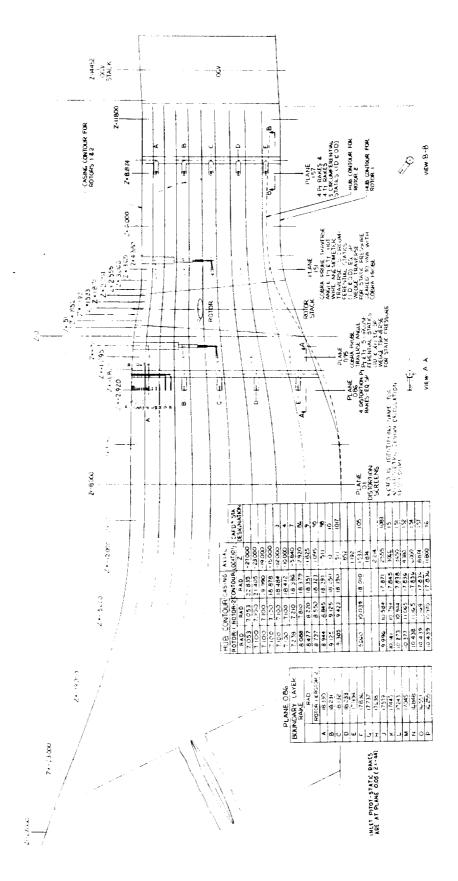


Figure 5. - Meridional view showing location of instrumentation.

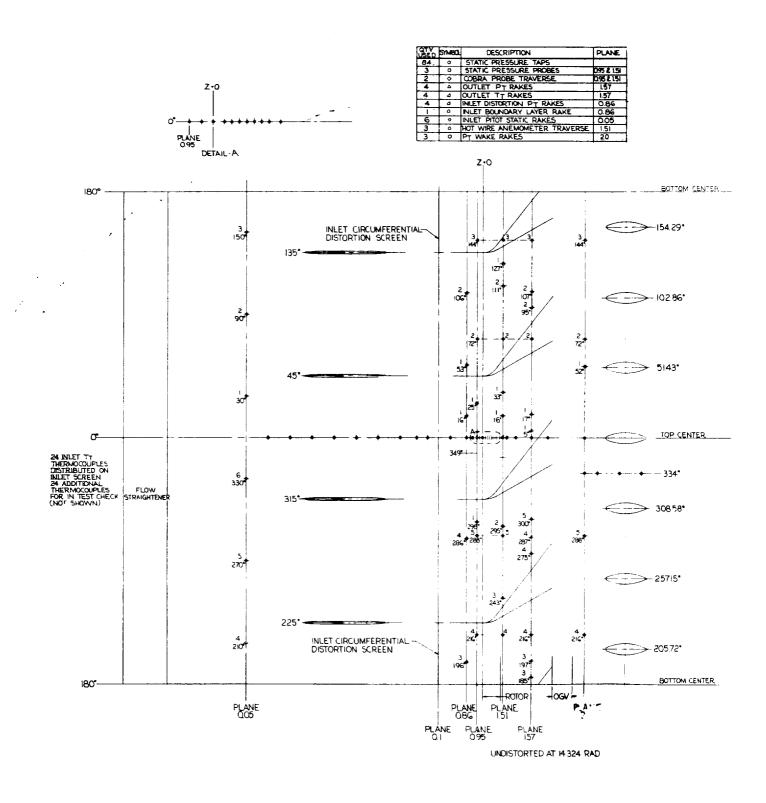
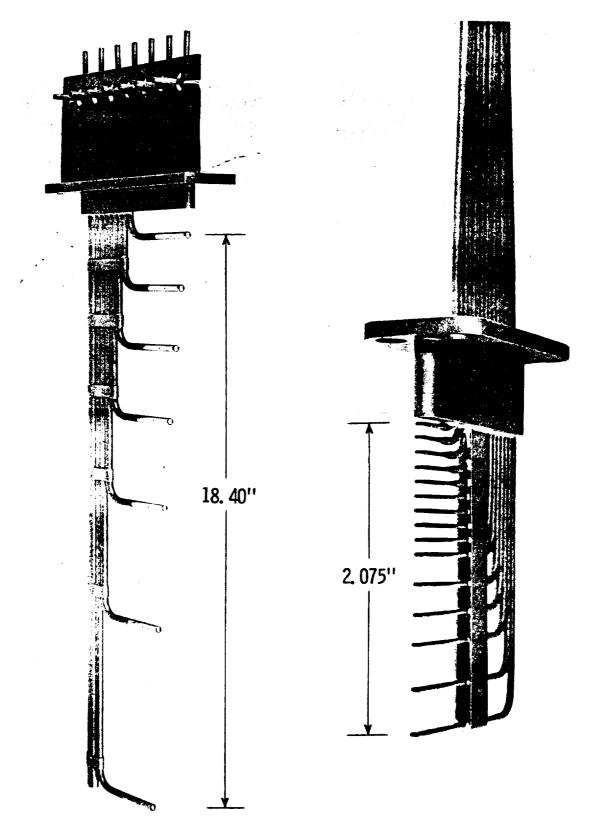


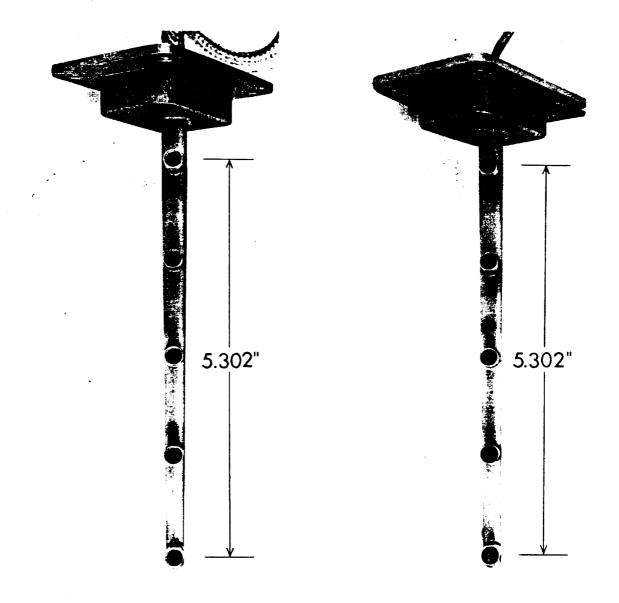
Figure 6. - Development showing circumferential location of instrumentation.



(a). - Inlet pitot-static rake.

(b). - Casing boundary layer rake.

Figure 7. - Photographs of fixed instrumentation.



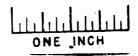
(c). Discharge total temperature rake. (d). Discharge total pressure rake.

Figure 7. - Photographs of fixed instrumentation.





(a). - Shielded hot wire probe.



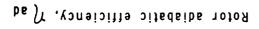


(b). - Cobra probe for sensing flow angle, total pressure and total temperature.



(c). - Wedge probe for sensing static pressure.

Figure 8. - Photographs of traverse instrumentation.



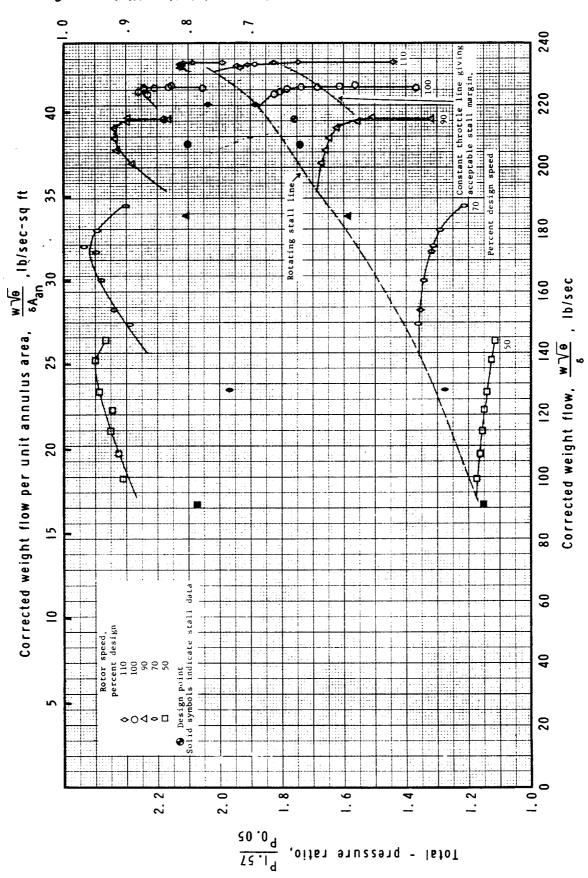
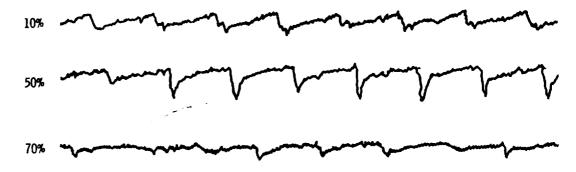


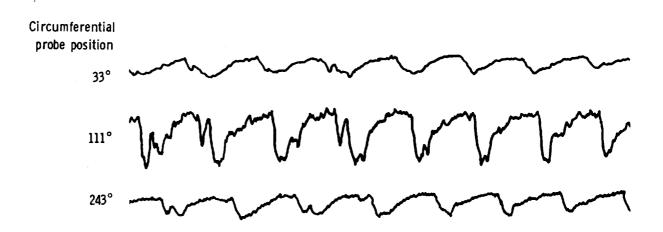
Figure 9. - Rotor performance map.

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Immersion



(a) Sample of hot wire anemometer traces at 90 percent design rotor speed.

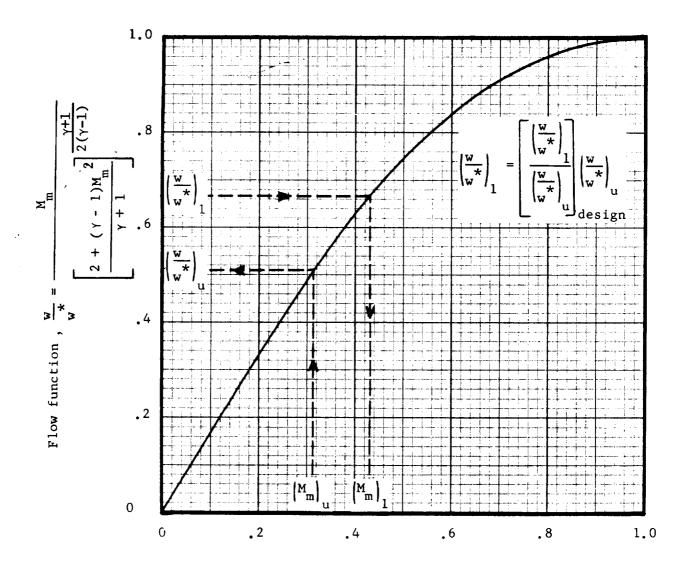


(b) Sample of hot wire anemometer traces from 10 percent immersion at 90 percent design rotor speed.

Rotor speed, percent design	Number of stall cells	Stall cell speed Rotor speed	Radial extent of stall cell	Throttle setting at stall
50	2	. 68	Full span	4. 10
70	3	. 69	Full span	5. 45
90	1	. 59	Full span	8. 4 5
100	1	. 61	Full span	10. 10
110	1	. 61	Full span	10, 70

(c) Tabulation of stall data

Figure 10. - Sample hot-wire traces and tabulation of stall data.



Meridional Mach number , M_m

Figure 11. - Relationship between flow function and meridional Mach number - used for transferring traverse measurements to blade edges.

Dashed lines with arrows and inset formulas indicate calculation sequence for sample case at leading edge.

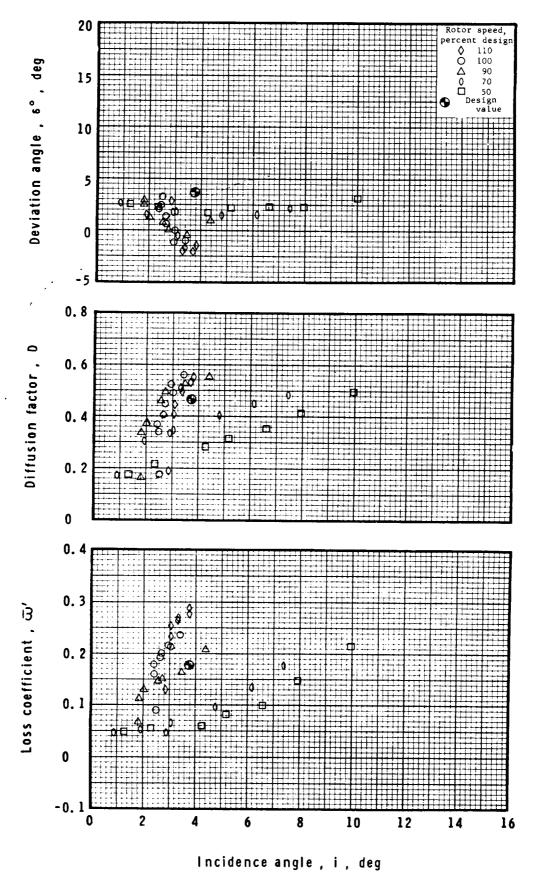


Figure 12(a). - Blade element data measured at 10% immersion from tip.

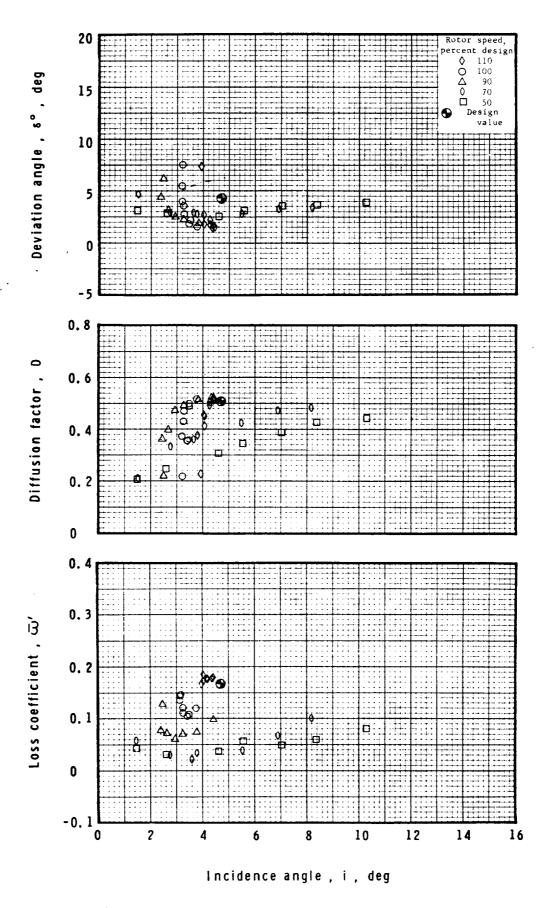


Figure 12(b). - Blade element data measured at 30% immersion from tip.

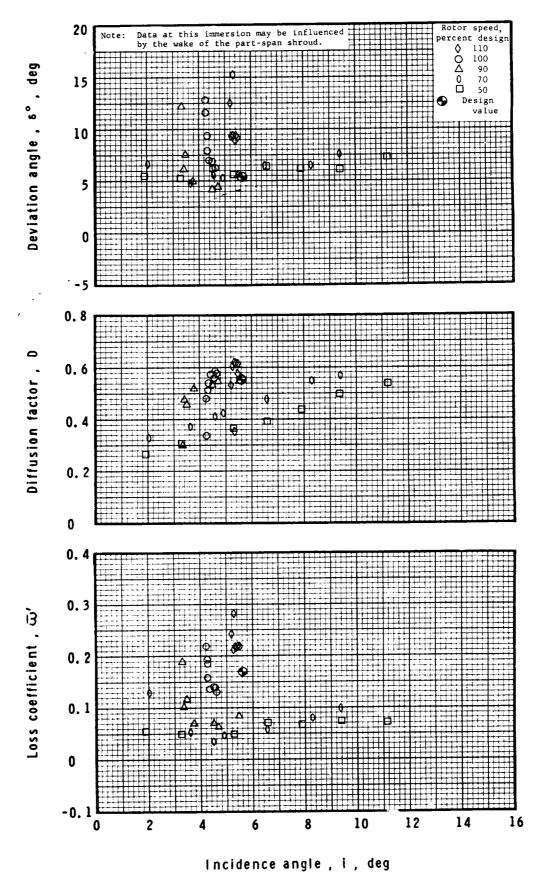


Figure 12(c). - Blade element data measured at 50% immersion from tip.

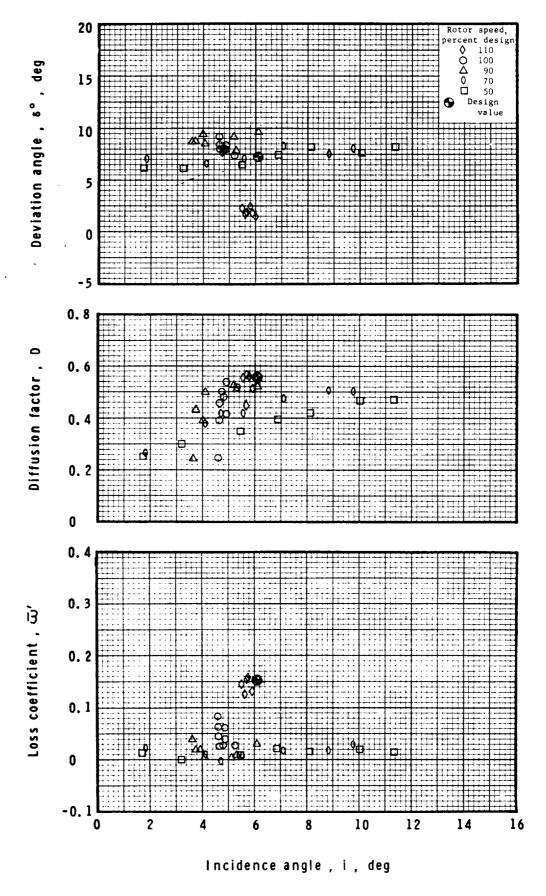


Figure 12(d). - Blade element data measured at 70% immersion from tip.